



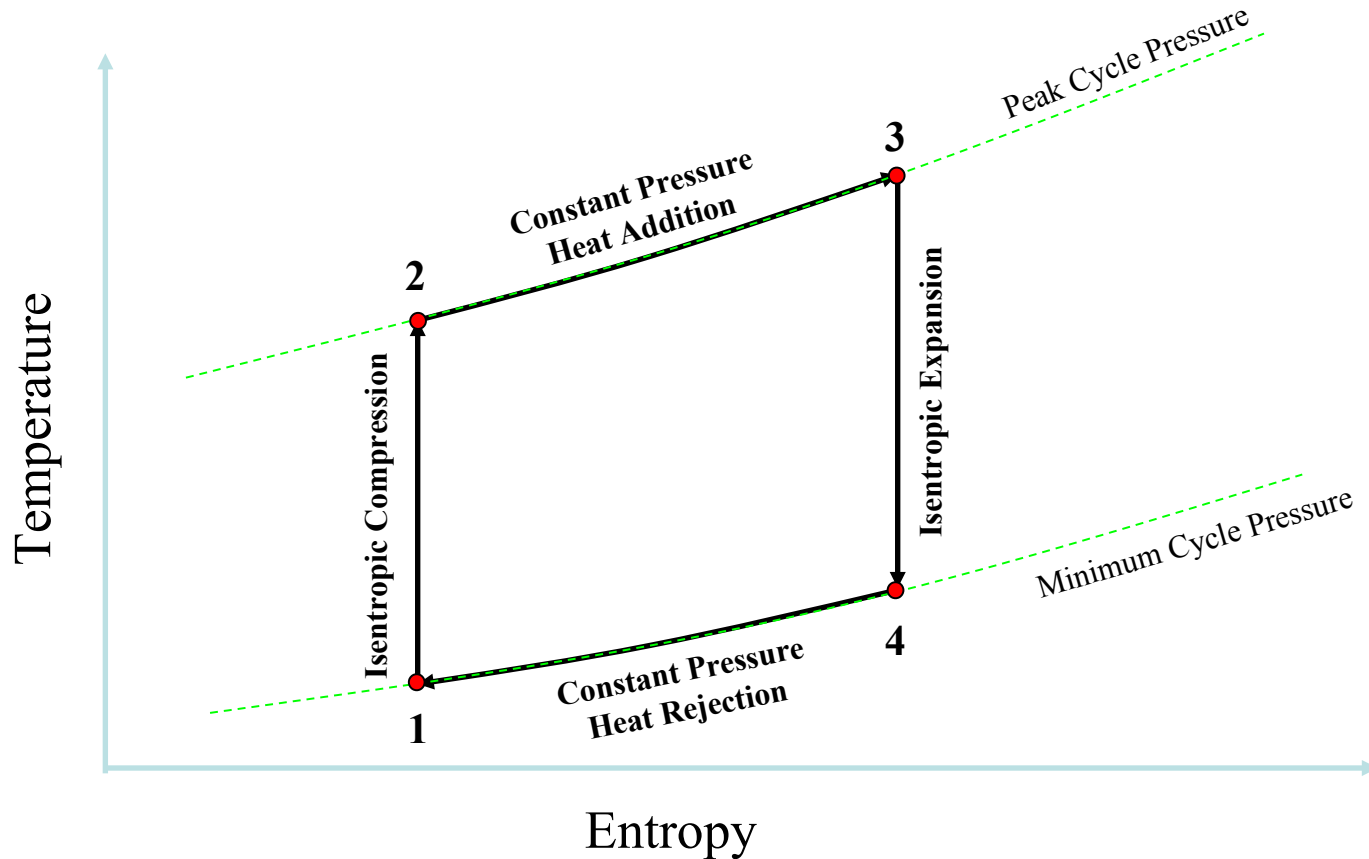
Thermodynamics Overview

Contents

- Brayton Cycle Basics
- Flow Parameter
- Cycle Deck
- Firing Temperature
- Control Curve

Ideal Brayton Cycle

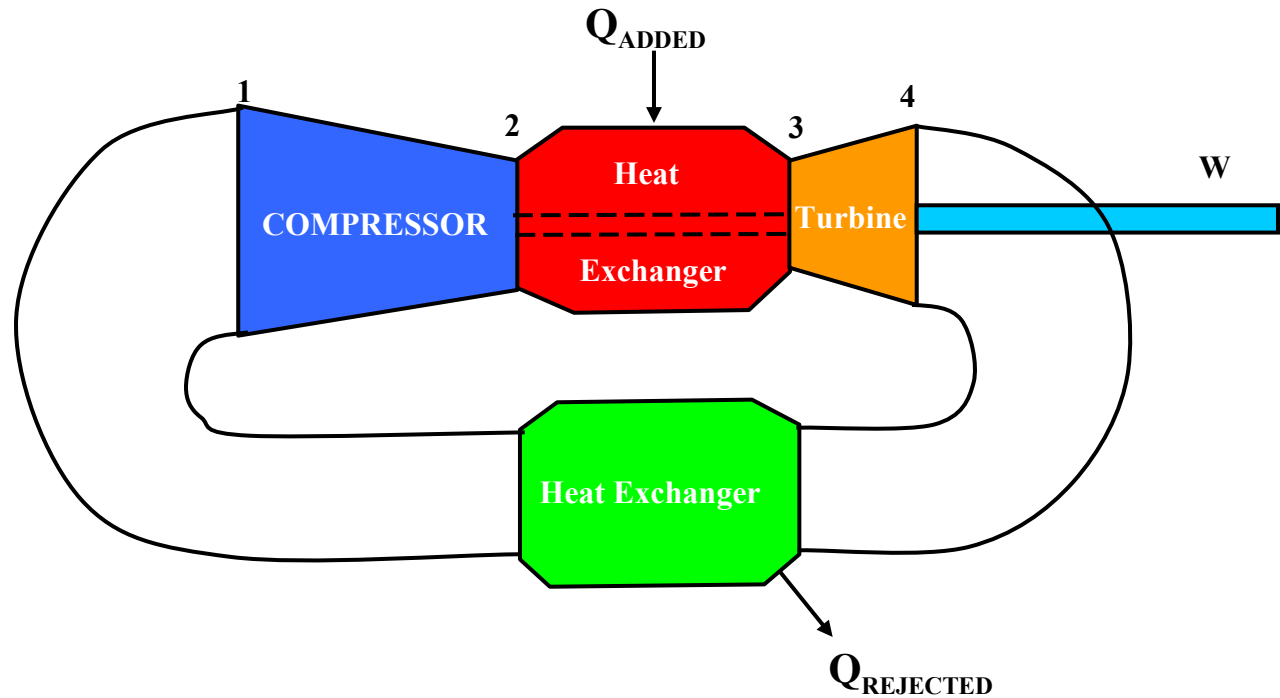
Four Thermodynamic Processes



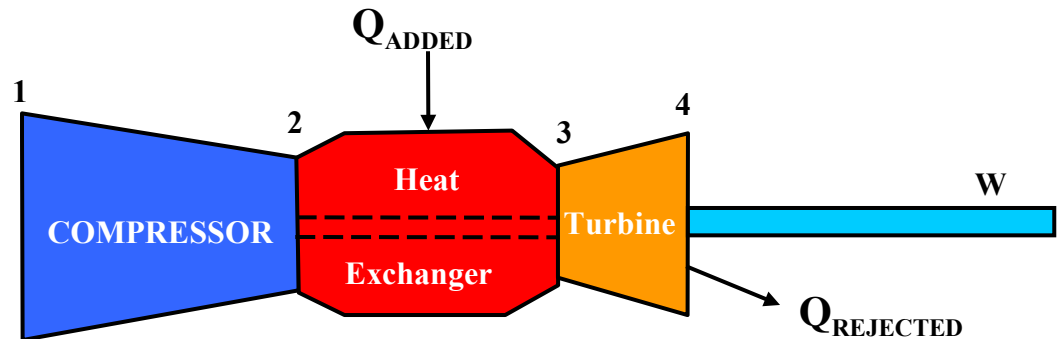
Brayton Cycle

Gas Turbine Application

CLOSED
CYCLE



OPEN
CYCLE



Ideal Brayton Cycle

Cycle Efficiency

Definition:

$$\eta_{\text{Cycle}} = \frac{\text{Work Output}}{\text{Heat Added}} = \frac{(T_3 - T_4) - (T_2 - T_1)}{(T_3 - T_2)}$$

Re-Arranging and Substitution Using:

$$\eta_{\text{Cycle}} = 1 - \frac{1}{\left(\frac{P_2}{P_1}\right)^{\gamma-1/\gamma}} \quad \frac{P_2}{P_1} = \left(\frac{T_2}{T_1}\right)^{\gamma/\gamma-1} = \frac{P_3}{P_4} = \left(\frac{T_3}{T_4}\right)^{\gamma/\gamma-1}$$

Yields Cycle Efficiency = f (P_2/P_1):

$$\eta_{\text{Cycle}} = 1 - \frac{1}{\left(\frac{P_2}{P_1}\right)^{\gamma-1/\gamma}}$$

Brayton Cycle

Other Considerations

- Maximum Allowable Cycle Temperature
 - Material Limitations
 - Cooling Technologies
- Optimum Work Output
 - Selection of Design Pressure Ratio
- Non-Ideal Cycle Effects
 - Compression/Expansion Inefficiencies
 - Pressure Losses
 - Parasitic Flows

Ideal Brayton Cycle

Optimum Work – Selection of Pressure Ratio

Work Output:

$$W = C_P \left[(T_3 - T_4) - (T_2 - T_1) \right]$$

Isentropic Relationships yield:

$$T_4 = T_3 \left[\frac{T_1}{T_2} \right] \quad \text{when} \quad \frac{P_3}{P_4} = \frac{P_2}{P_1}$$

Differentiate with respect to T2:

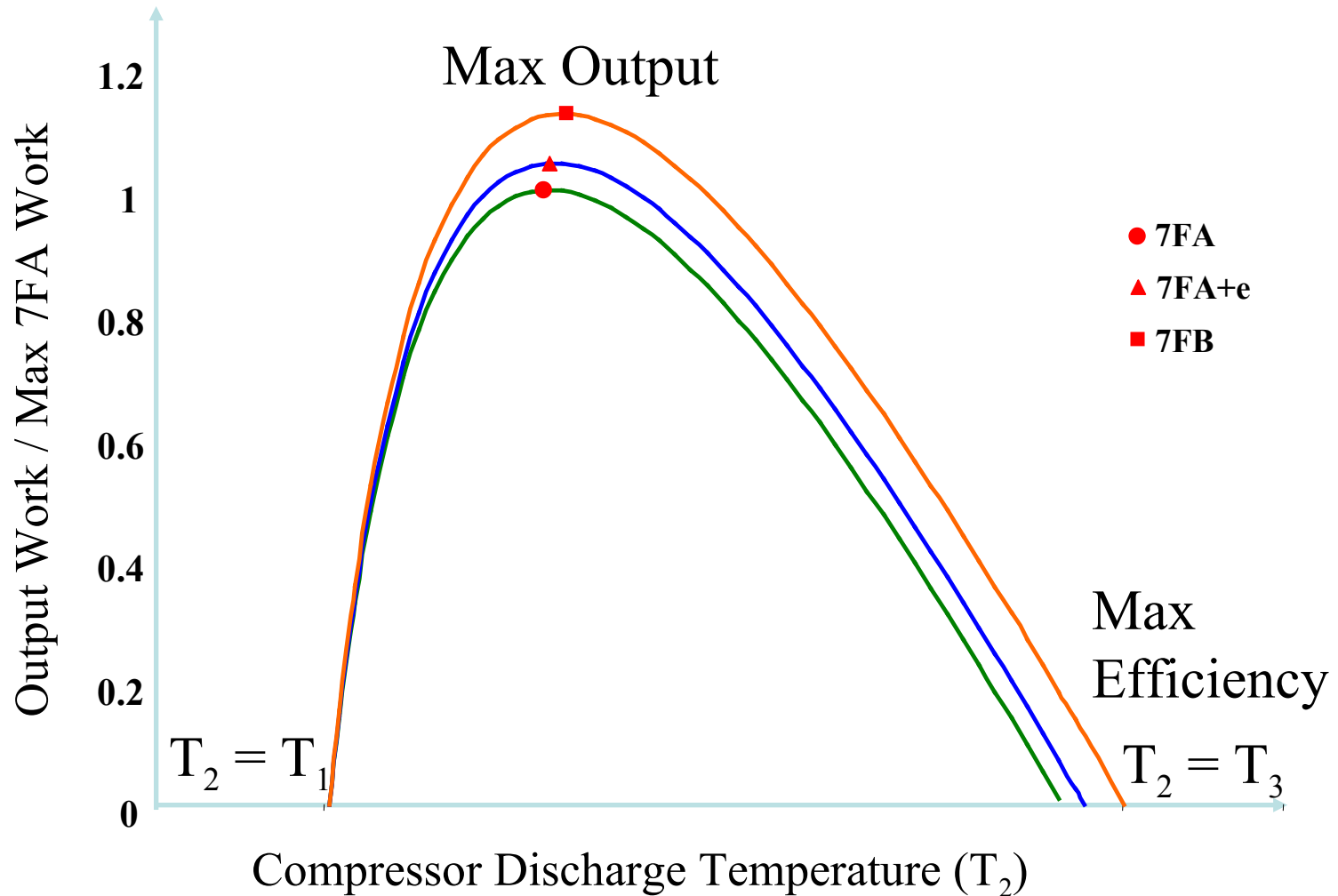
$$\frac{dW}{dT_2} = C_P \left[0 + \frac{T_3 T_1}{T_2^2} - 1 + 0 \right]$$

Set to Zero and Solve for T2:

$$T_2 = \sqrt{T_3 T_1}$$

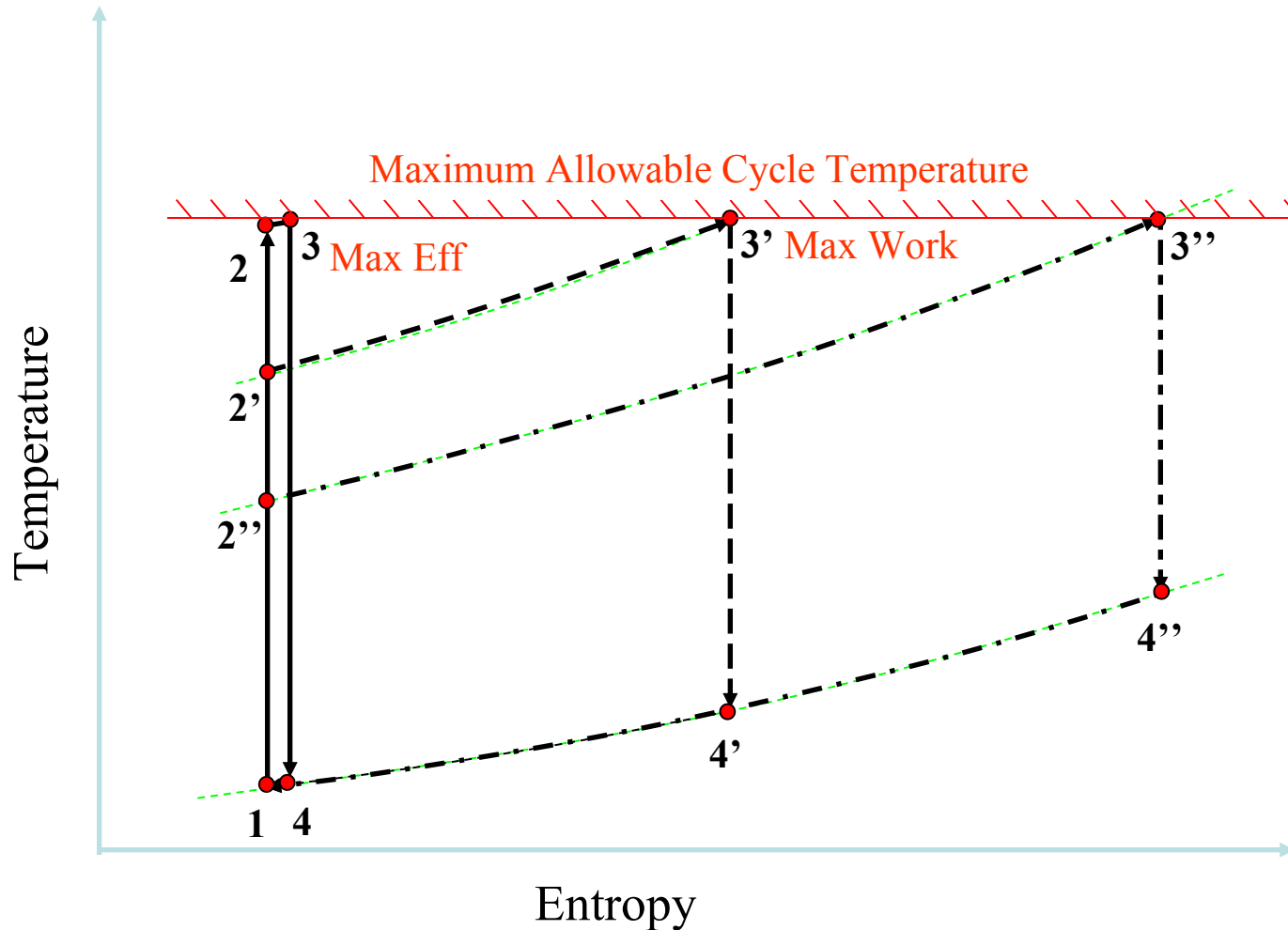
Ideal Brayton Cycle

Normalized Output Work vs. T_2 with Lines of Constant T_1 and T_3



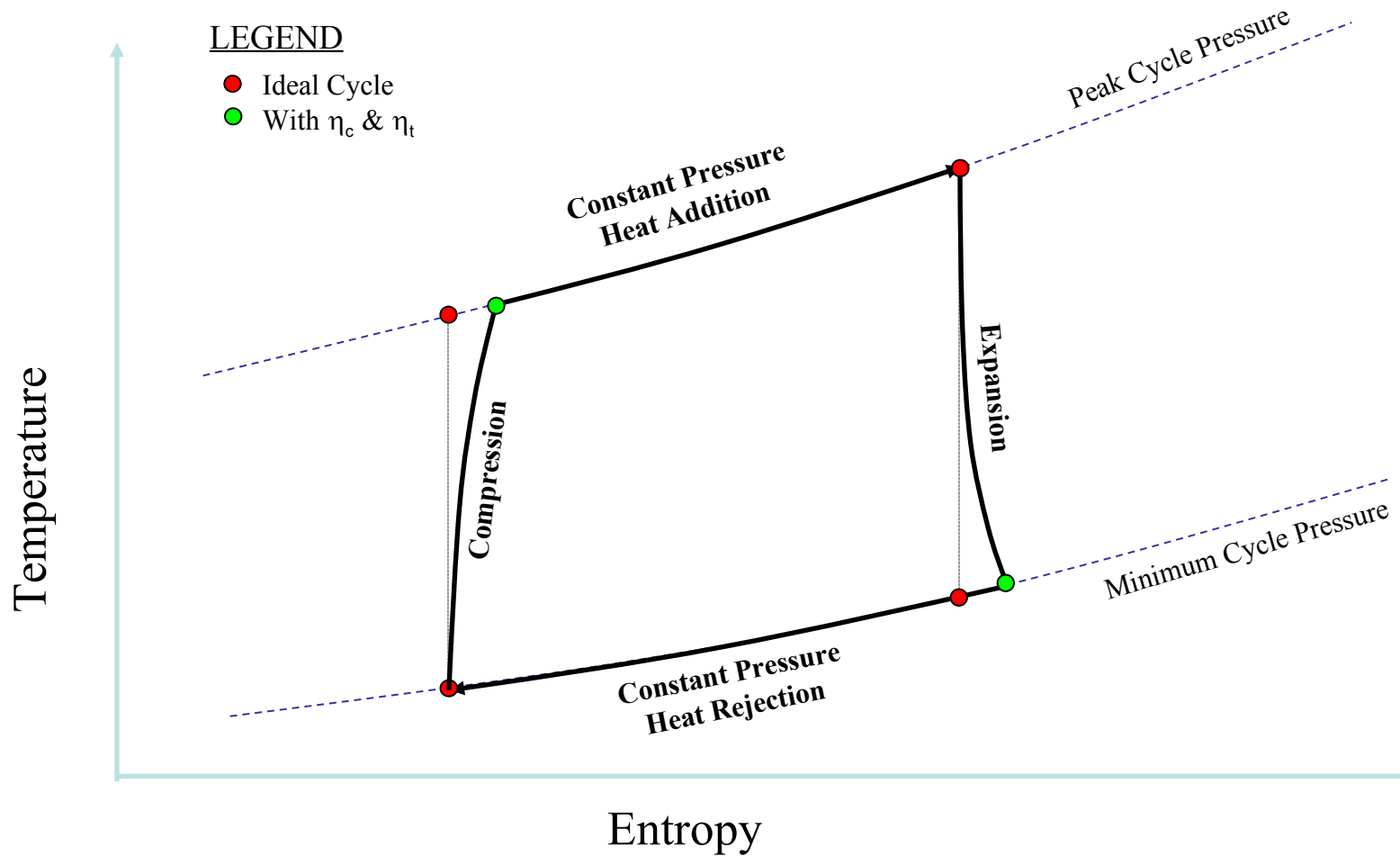
Ideal Brayton Cycle

Maximum Work vs. Maximum Efficiency



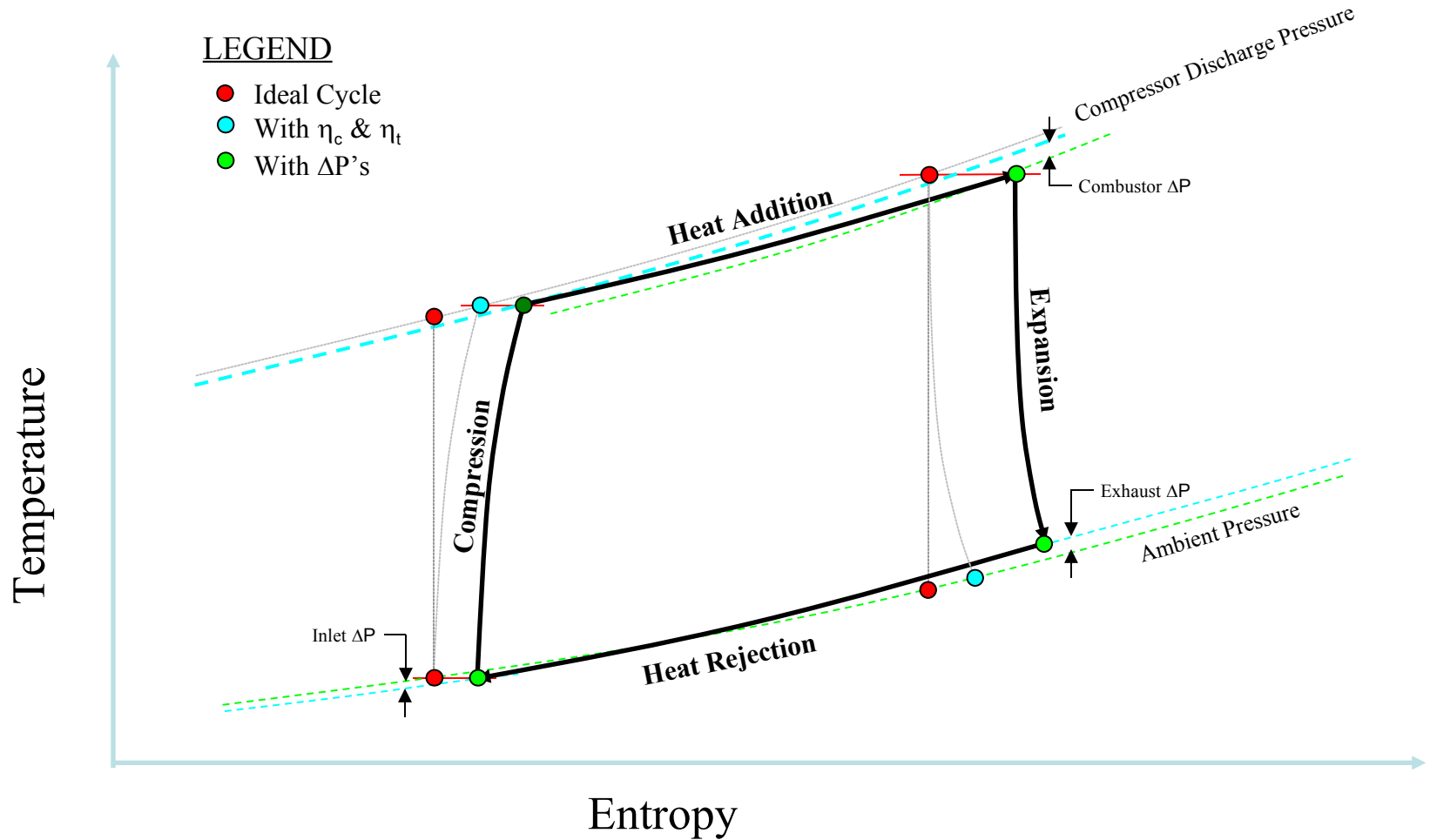
Brayton Cycle

Compression and Expansion Inefficiencies



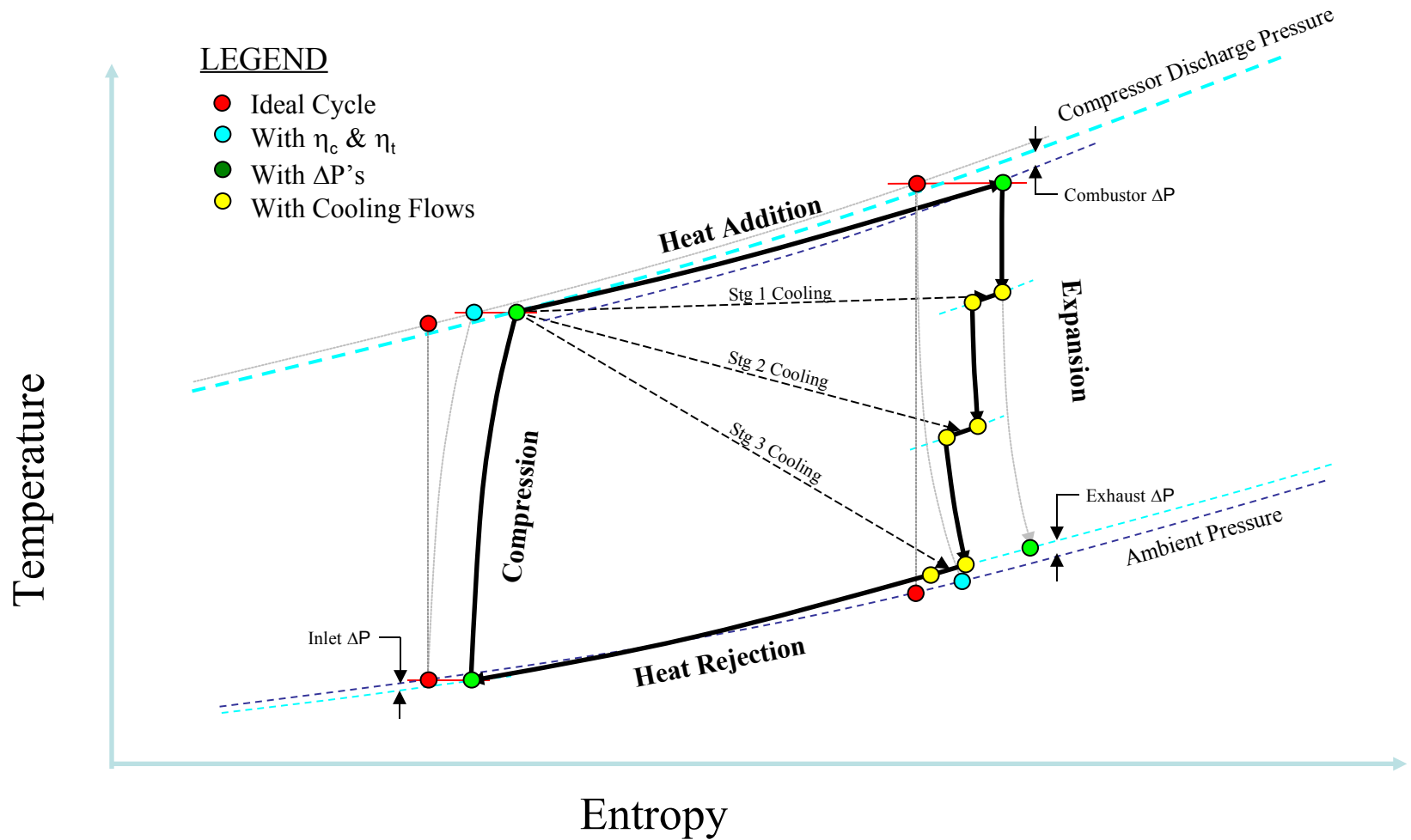
Brayton Cycle

Pressure Losses - Inlet, Combustor, Exhaust



Brayton Cycle

Parasitic Flows for Turbine Cooling



Flow Parameter - Defined

Starting from basic continuity equation:

$$W = \rho \times A \times V$$

Through substitution of thermo & compressible flow principles, then re-arranging terms:

$$\frac{W \sqrt{T_0}}{P_0 A} = \sqrt{\frac{\gamma}{R}} M \frac{\sqrt{1 + \frac{\gamma - 1}{2} M^2}}{\left(1 + \frac{\gamma - 1}{2} M^2\right)^{\frac{\gamma}{\gamma - 1}}}$$

Flow Parameter - Applied

Setting $M = 1$ (Choked Flow at Station 3)

$$\frac{W \sqrt{T_3}}{P_3 A_3} = \text{Const}$$

Given:

Machine Size $\propto W$

Technology $\rightarrow T_3$

Max Output $\rightarrow P_3$

A_3 is set to hold continuity

Brayton Cycle General Observations

- For Ideal Cycle

- Cycle efficiency increases with P_2/P_1 , and not dependent on T_3
- For given P_2/P_1 , as T_3 increases, all additional energy input becomes work output

- For Real Cycle

- (T_3 at Zero Work)Real > (T_3 at Zero Work)Ideal
- As T_3 increases, both cycle efficiency & work output increase
- Therefore, general conclusion is higher T_3 is good

Gas Turbine Performance Estimator (Cycle Deck)

Customers can register and then download
GTP Estimator by going to:

<http://www.gepower.com/home/index.htm>

Address  <http://www.gepower.com/home/index.htm>

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Technical Library



GTP (Cycle Deck) - The Primary Gas Turbine Thermodynamic Tool

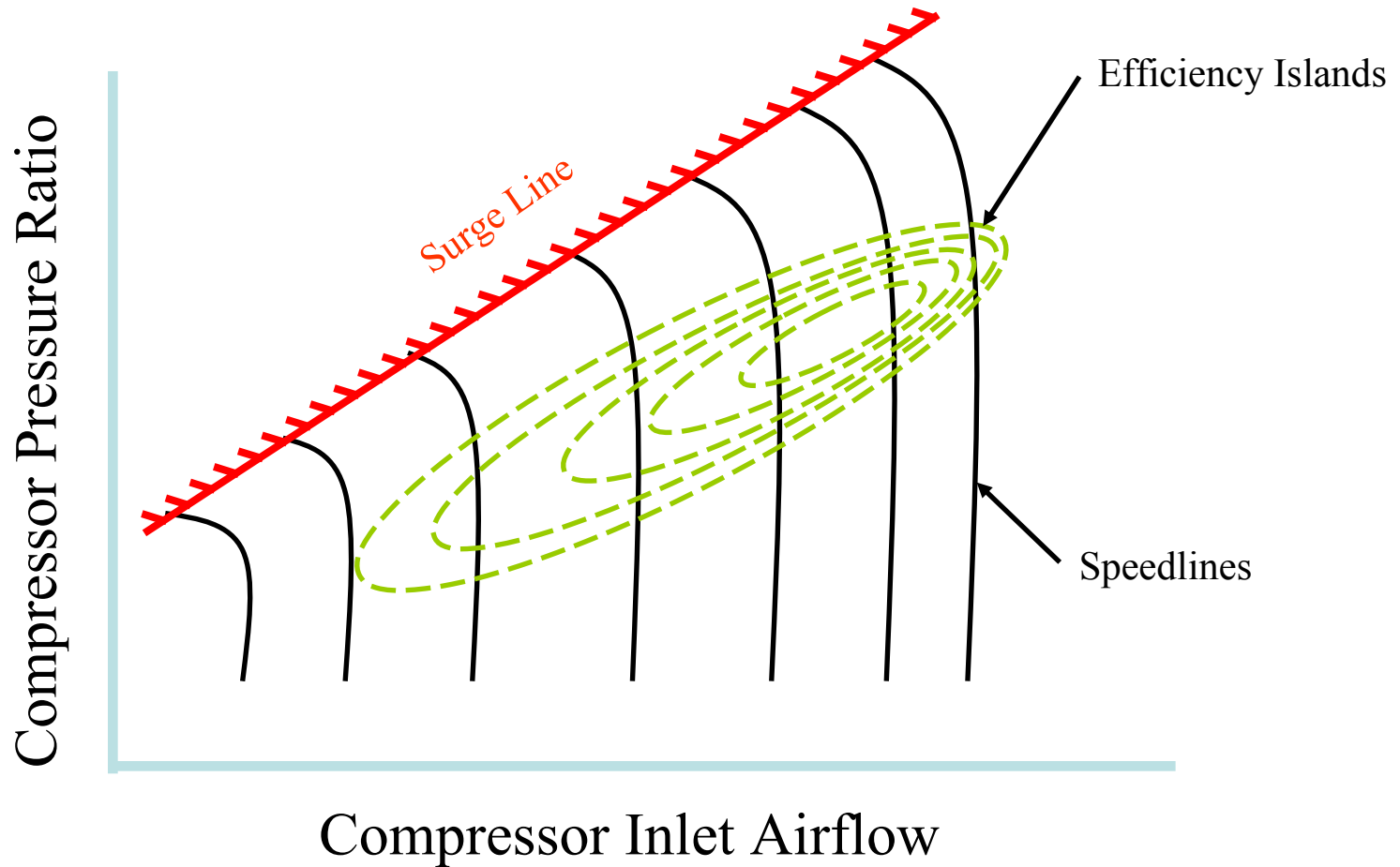
- An aero-thermal math model of the entire GT cycle (Thermodynamics, Aerodynamics, Compressible Flow, Heat Transfer)
- Built & maintained by Systems Engineering
- Uses:
 - Boundary conditions for component designers
 - Performance prediction (Guarantees, Correction Curves, Studies)
 - Control schedule development (T_x Control, IGV Control, etc.)
 - Data reduction/analysis
 - Core of performance monitoring programs

GTP (Cycle Deck) - Modular

	Module	Inputs	Outputs
Control System & Iteration & Convergence	Inlet System	• Ambient Conditions • Inlet ΔP • IBH Functionality	• Compressor Inlet Conditions
	Compressor	• Rotational Speed • Pressure Ratio • IGV Angle	• Inlet/Exit Flow Rate • Overall Efficiency • Compressor Exit & Extraction Point Conditions
	Parasitic Flows	• Compressor Flow Conditions • Design Cooling Flow Fractions • Flow Parameter Characteristic	• Flow Rate Down Each Circuit
	Combustor	• Compressor Exit Conditions • Fuel & Diluent Flow & Composition • Design Point $\Delta P/P$	• $\Delta P/P$ • Combustor Exit Gas Conditions & Composition • Nox & CO
	Turbine	• Combustor Exit Conditions • Dilution Air Proportions	• Stage by Stage Exit Conditions • Bucket Relative Temperatures
	Exhaust System	• Turbine Exit Conditions • Design Point ΔP	• $\Delta P/P$
	Generator	• Shaft Power • Power Factor	• Generator Electrical Losses • Electrical Power Output
	Cycle Performance	• Flows, Enthalpies Throughout Cycle	• Power Output, Heat Rate, Cycle Efficiency

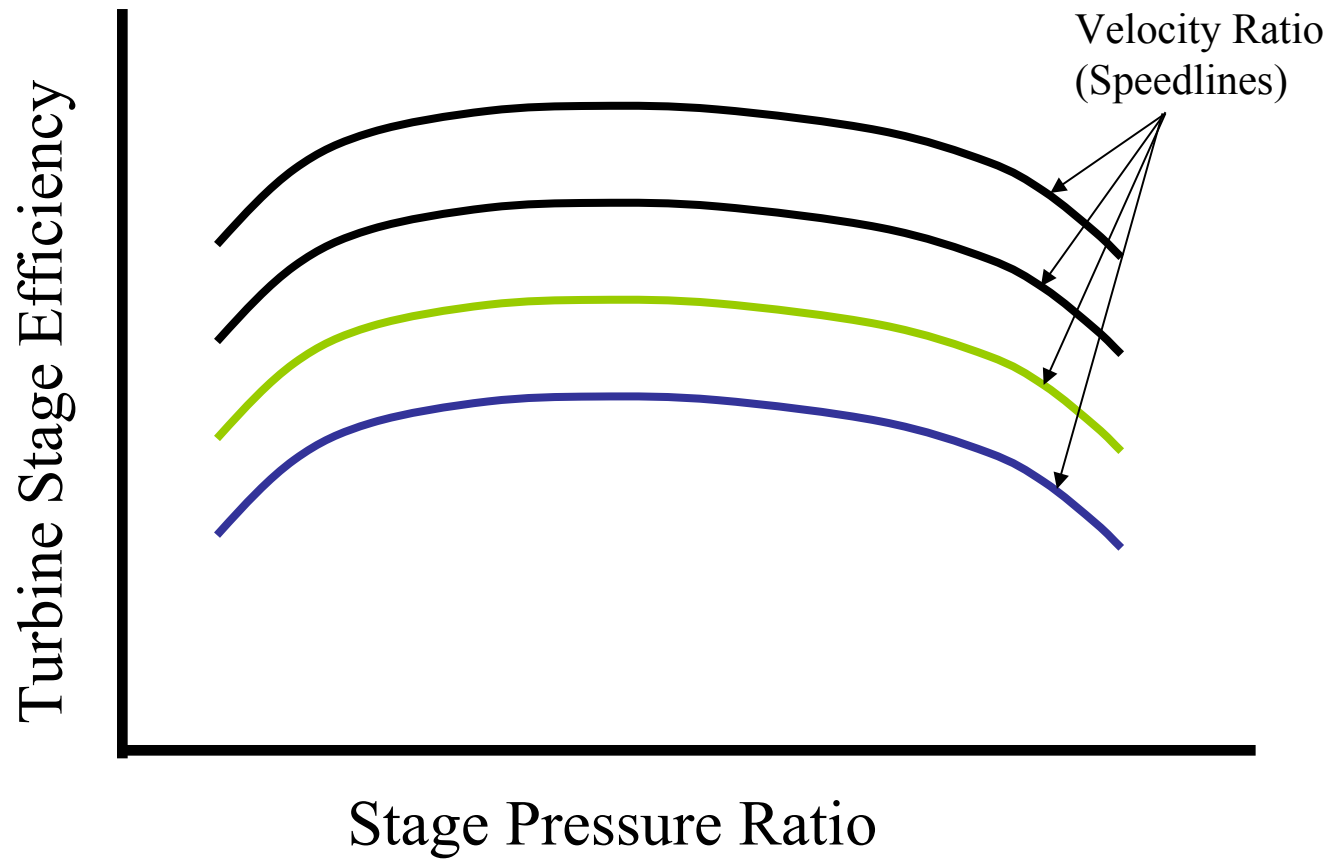
GTP (Cycle Deck)

Compressor Map



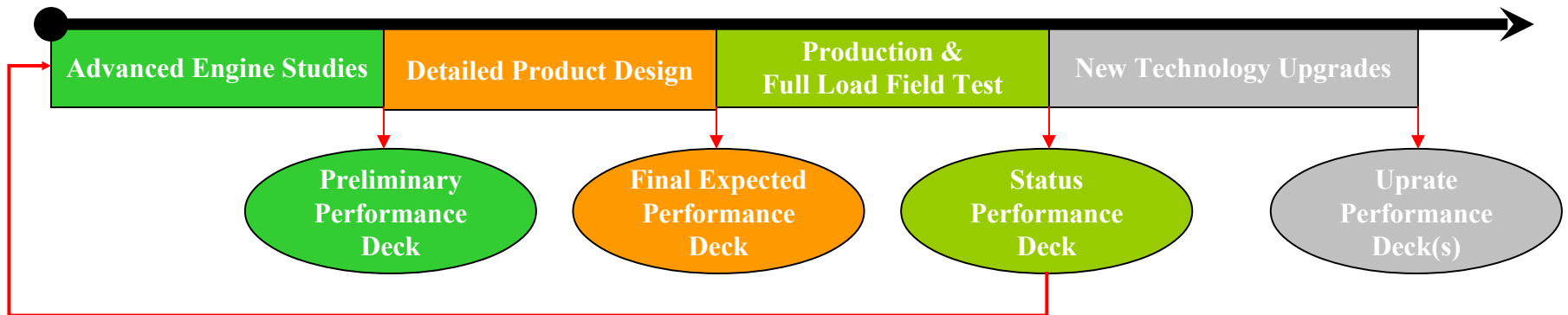
GTP (Cycle Deck)

Turbine Map



GTP (Cycle Deck)

Four Stage Life Cycle

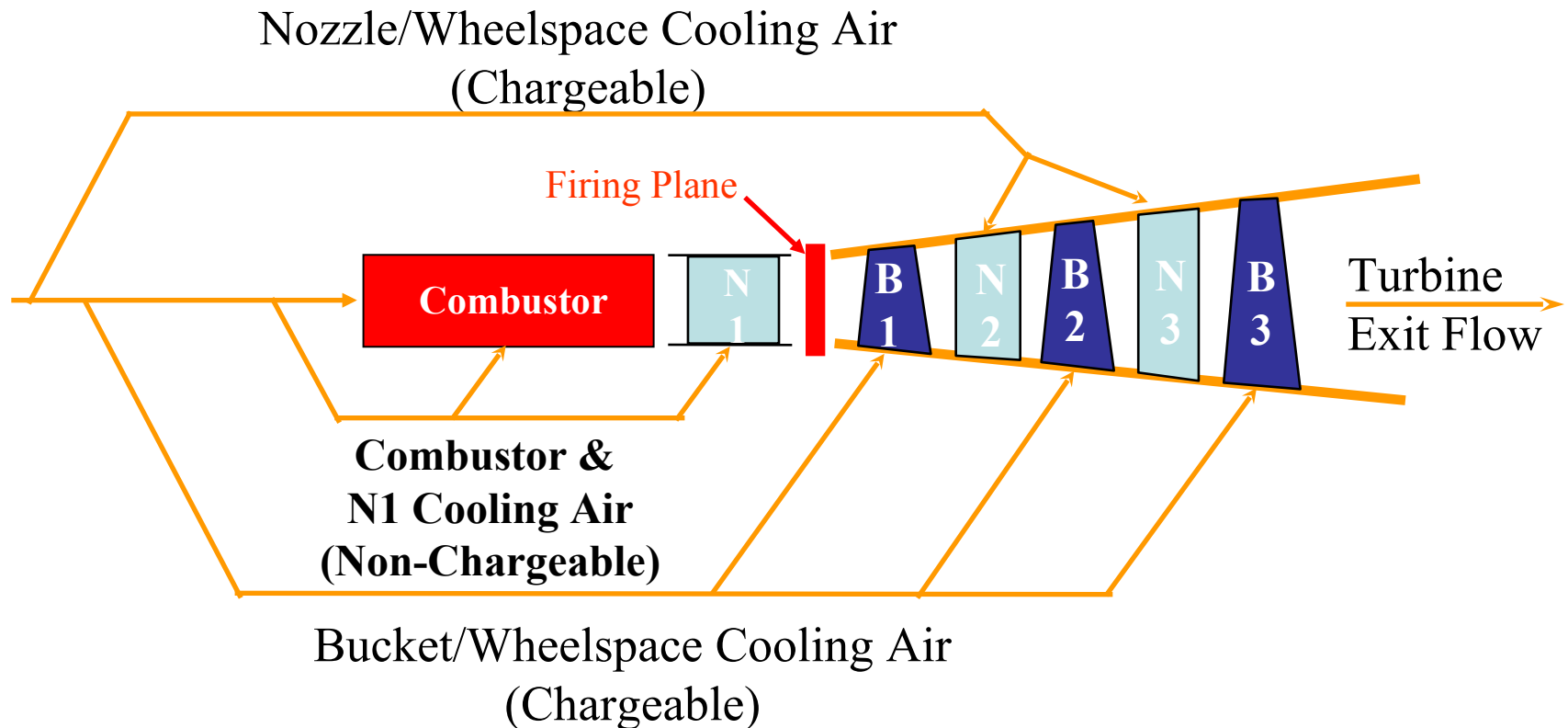


Firing Temperature

- Defined as gas temp at point in cycle where initiation of turbine work begins (N1 trailing edge / B1 leading edge)
- Highest temp point in cycle for thermal performance, but not hottest point in cycle
- Not possible to measure precisely
- Usually the “target parameter” for T_x control curve generation, but not always

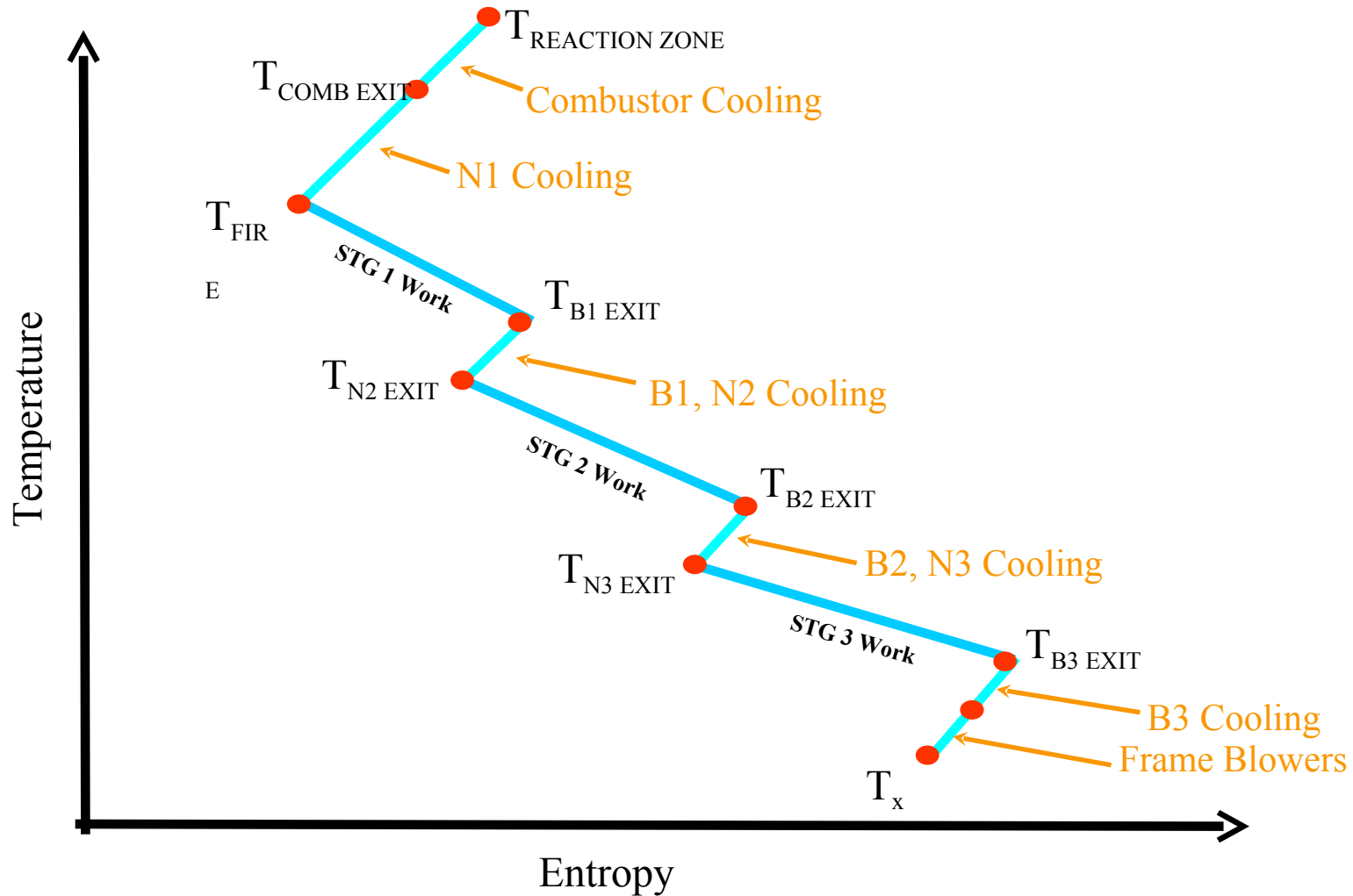
Firing Temperature

Defined at N1 Trailing Edge



Expansion Line

Turbine Cooling Air (Chargeable vs Non-Chargeable)



Temperature Control Curve

- T_x control used to regulate fuel flow such that gas temps/parts lives conform to design basis
- Subject to knowledge of turbine efficiency, turbine cooling flows, back pressure
- Can have separate curves for base load, part load
- Can be tailored to achieve variable firing temperature, simultaneously meeting performance, emissions, & parts life goals

Temperature Control Curve

Strategy Based on Turbine Efficiency Equation

Starting From Basic Efficiency Equation:

$$\eta_{\text{turbine}} = \frac{\Delta T}{\Delta T'}$$

Through substitution of thermo & compressible flow principles, then re-arranging terms:

$$T_3 = \frac{T_4}{\left[1 - \eta_{\text{turbine}} \left(1 - \frac{1}{\left(\frac{P_3}{P_4} \right)^{\gamma-1/\gamma}} \right) \right]}$$

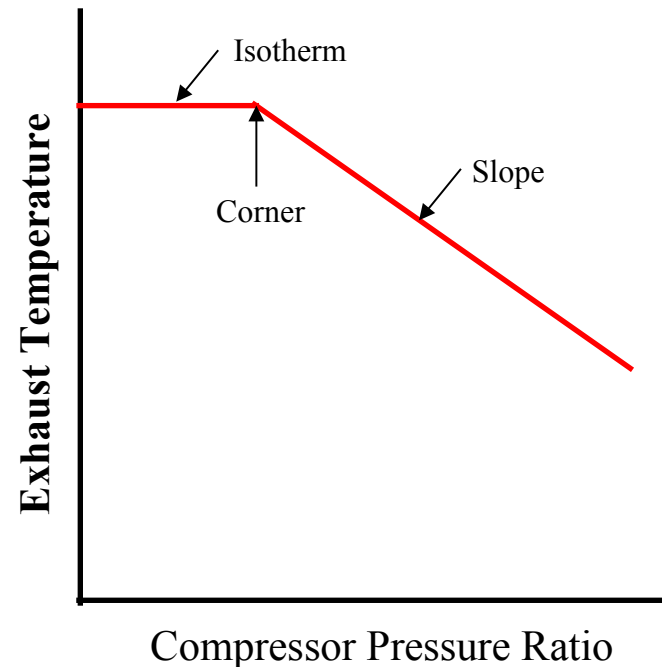
Temperature Control Curve

Design Process

Process Inputs:

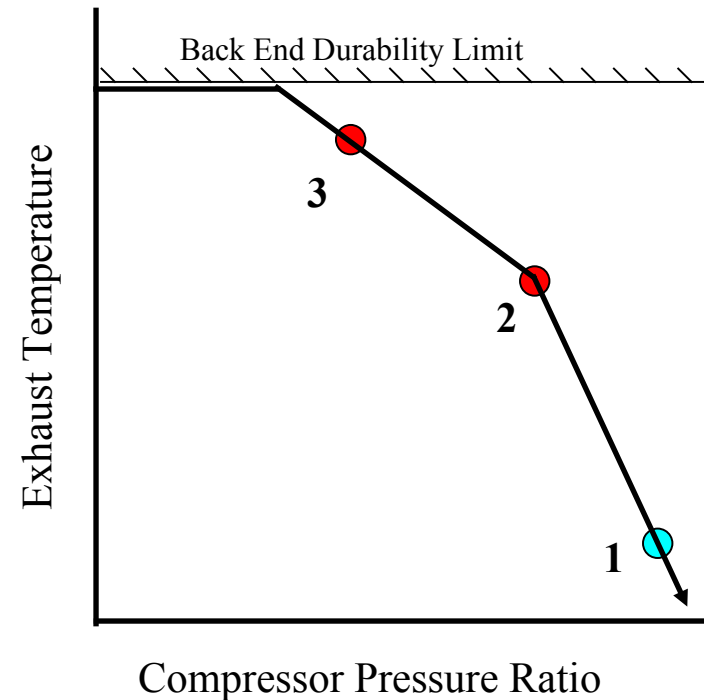
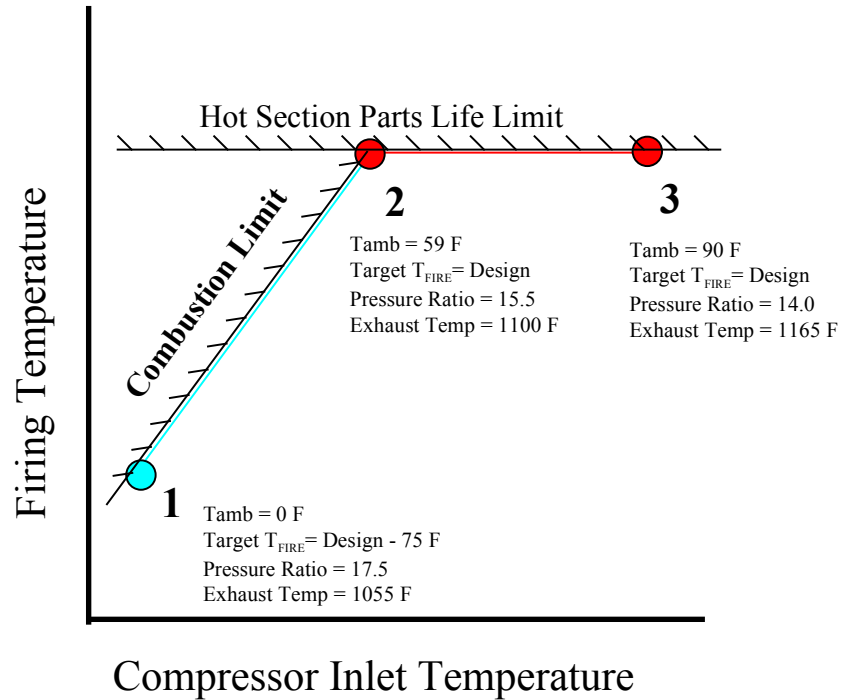
- 1) Current Cycle Deck
- 2) Target Firing Temperature
- 3) Expected Site Ambients
- 4) Expected Fuel
- 5) Target N_{OX}
- 6) T_x Limit
- 7) “Special” Considerations
 - Tilted Curves
 - 1, 2, 3 Piece
 - Humidity
 - Dry vs Wet
 - DLN T_{RISE} Criteria
 - Base Load vs Part Load
 - Compressor Temp Bias

Process Output:



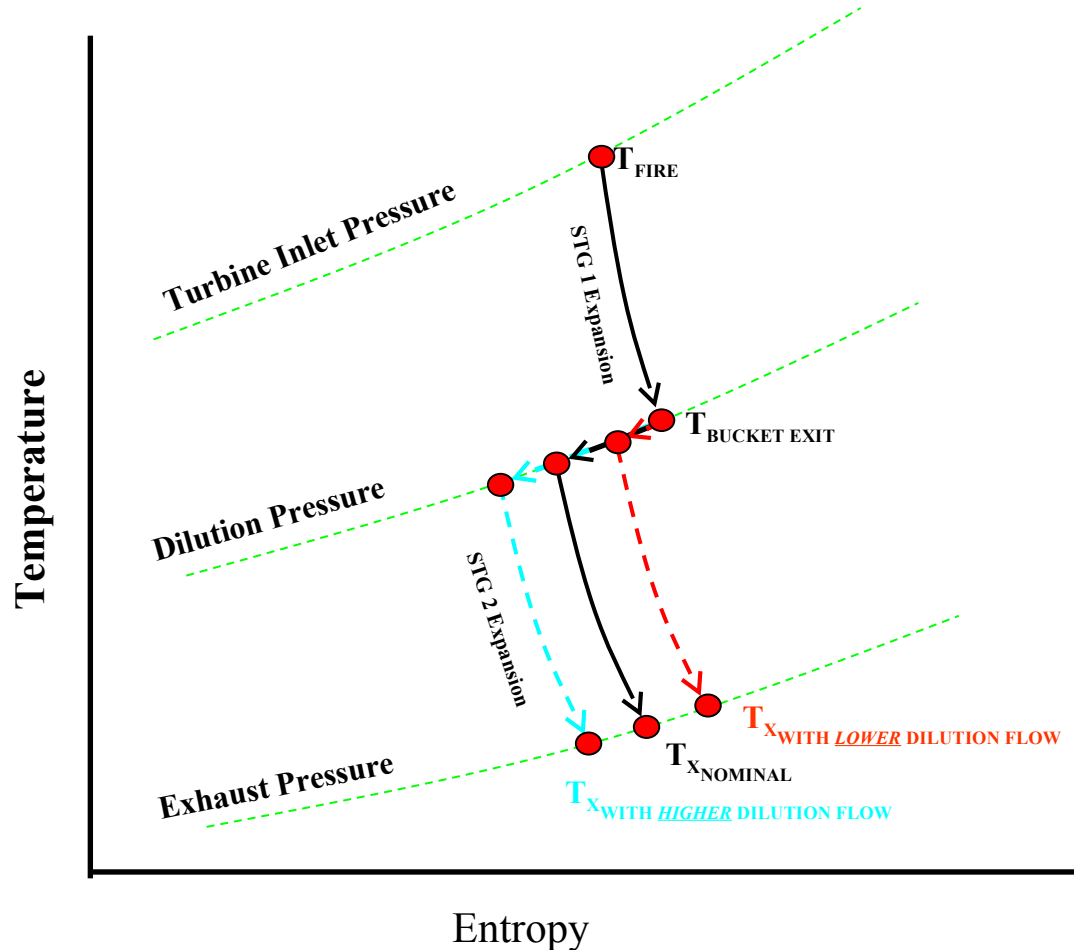
Temperature Control Curve

Design Example



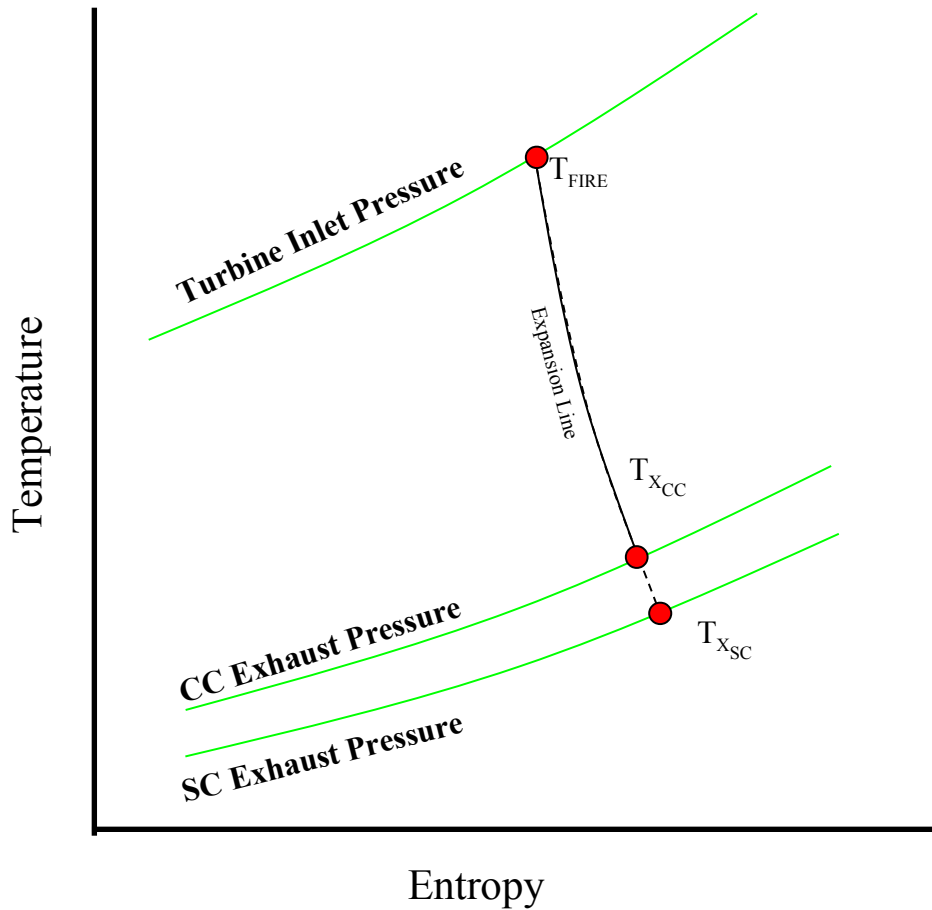
Temperature Control Curve

Dilution Effect



Temperature Control Curve

Backpressure Effect



Wrap - Up

- **Brayton Cycle Analysis**

- Higher P/P is Good
- Higher Firing Temp is Good
- Cycle Inefficiencies, DP's, Turbine Cooling are Bad

- **Cycle Deck**

- Modular Design, Evolves Over Time
- #1 Performance Tool (Design, Ratings, Control, Monitors)

- **Firing Temperature**

- Controlled via Exhaust Temperature
- Sensitive to hT , Turbine Cooling, Backpressure