# Solid-Liquid Separation in Water Treatment

Settling and Flotation

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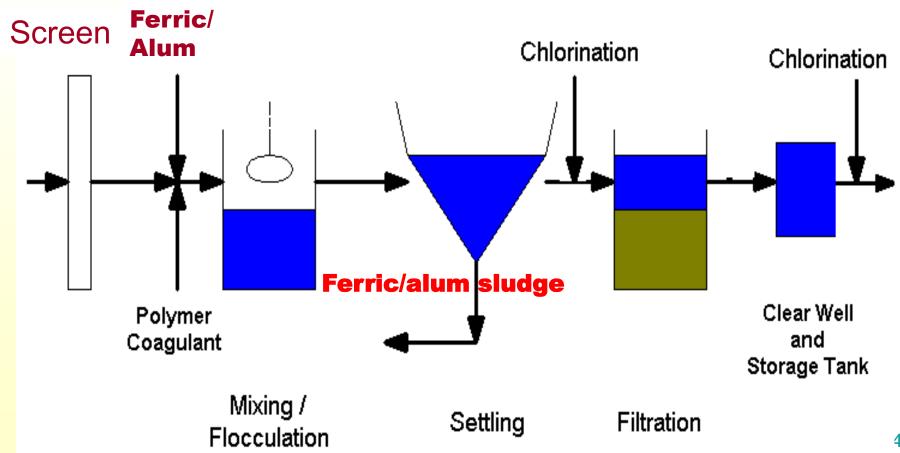
# Introduction

The need to clarify water Aesthetic and health reasons
Technologies available

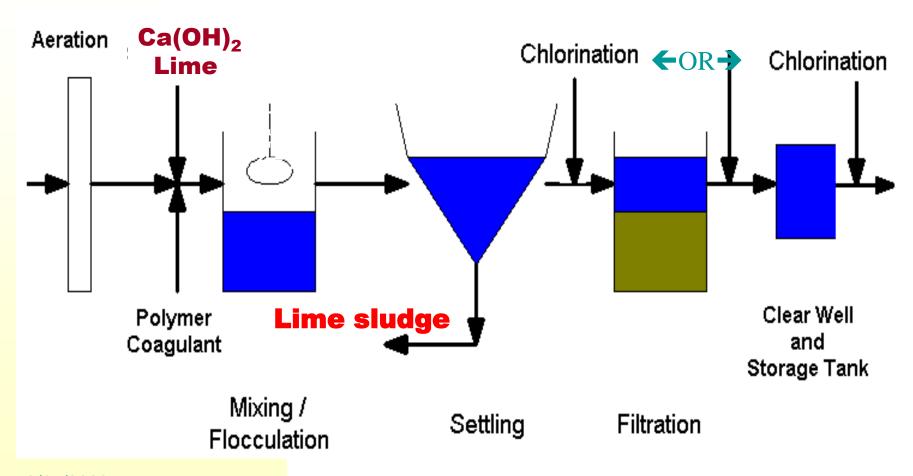
# **Topics of Discussion**

- Separation by settling
- Separation by flotation
- Direct filtration
- Softening

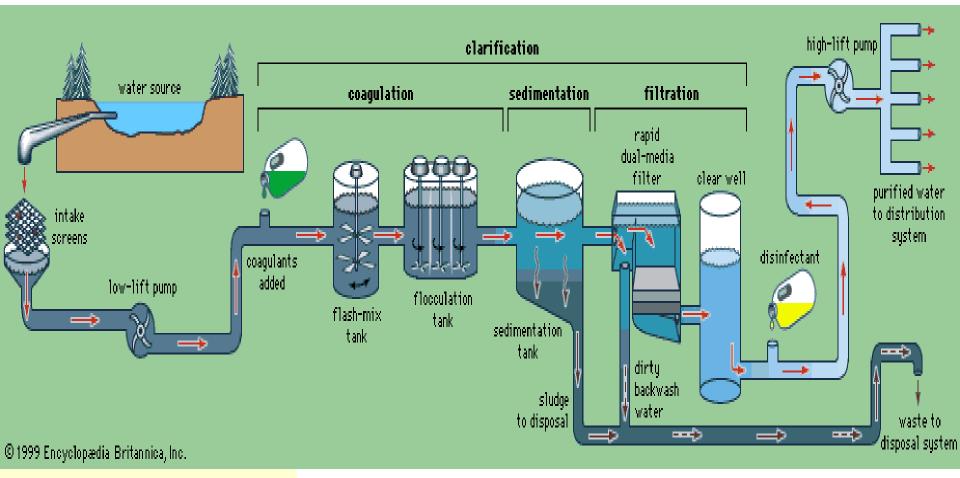
# **Typical surface water** treatment process



# Typical water treatment process with lime softening



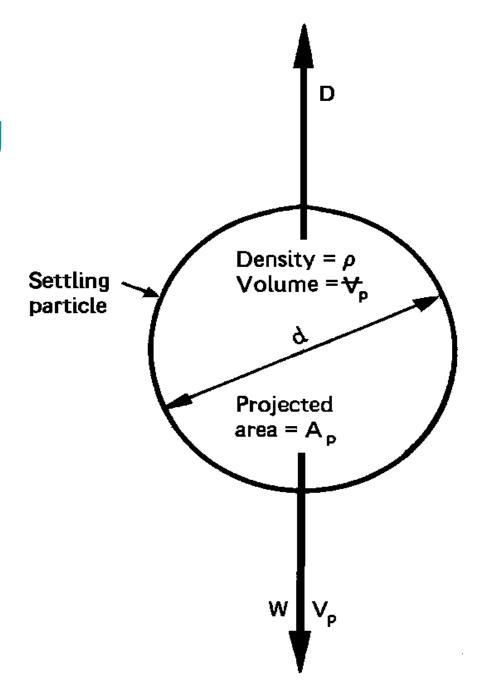
# Solid-liquid separation in water treatment



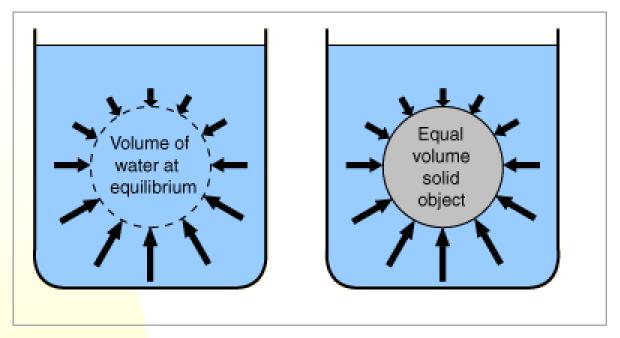
### Typical layout of a water treatment plant

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# Analysis of Forces Acting On a Settling Particle



# Archimedes's Principle



Examination of the nature of <a href="buoyancy">buoyant force on a volume of water and a submerged object of the same volume is the same. Since it exactly supports the volume of water, it follows that the buoyant force on any submerged object is equal to the weight of the water displaced. This is the essence of Archimedes principle.

#### **Terminal Velocity of a Particle**

An expression for  $V_t$  from the submerged weight of the particle,  $W_t$ , and the fluid drag force,  $D_t$ .

The drag force on a particle is given by

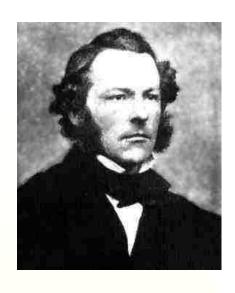
$$\mathbf{D} = \mathbf{C}_{\mathbf{D}} \rho_{/} \mathbf{A}_{\mathbf{p}} \mathbf{V}_{\mathbf{t}}^{2} / 2$$

The submerged weight of the particle can be expressed as

$$\mathbf{W} = (\rho - \rho_{i})\mathbf{g} \ \forall_{s}$$

**Since D = W,** the above, after substituting  $A_p$  and  $\forall_p$  for particle diameter d

$$V_{t} = \frac{\sqrt{4 (\rho - \rho_{i}) gd}}{\sqrt{3\rho_{i} C_{D}}}$$



#### Stokes's Law

$$R_e < 1, C_D = 24 / Re$$

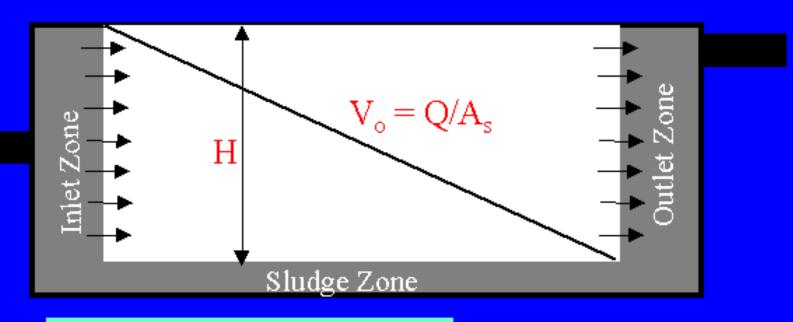
Substitute in the equation for v<sub>t</sub>

$$V_t = g (\rho - \rho_l) d^2$$
18  $\mu$ 

$$\mathbf{V_t} = \frac{2 (\rho - \rho_{\underline{\mathbf{l}}})gr^2}{9\mu}$$

The upflow velocity in a settling tank needs to be < V<sub>t</sub>

#### Sedimentation





$$v_o = \frac{H}{t_d} = \frac{H}{v/Q} = \frac{Q}{v/H} = \frac{Q}{A_s}$$

The overflow rate

#### Sedimentation

Typical design overflow rates for settling tanks are: 500-1000 gpd/ft<sup>2</sup> (20-40 m<sup>3</sup>m<sup>-2</sup>d<sup>-1</sup>)

All particles with a settling velocity greater than or equal to the overflow rate will be 100% removed.

Particles with a lesser settling velocity will be removed to a fractional extent. Those that happen to enter the settling zone near the bottom will be completely removed and those that enter near the top will not.



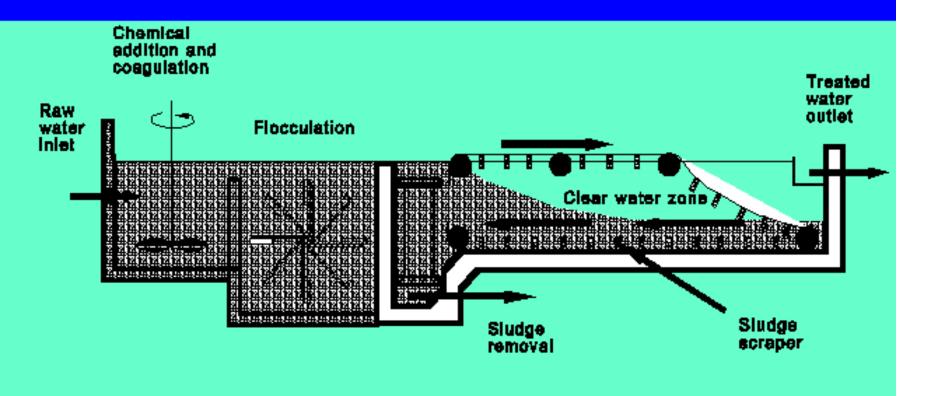
Fraction Removed = 
$$\frac{v}{\frac{Q}{A_s}}$$

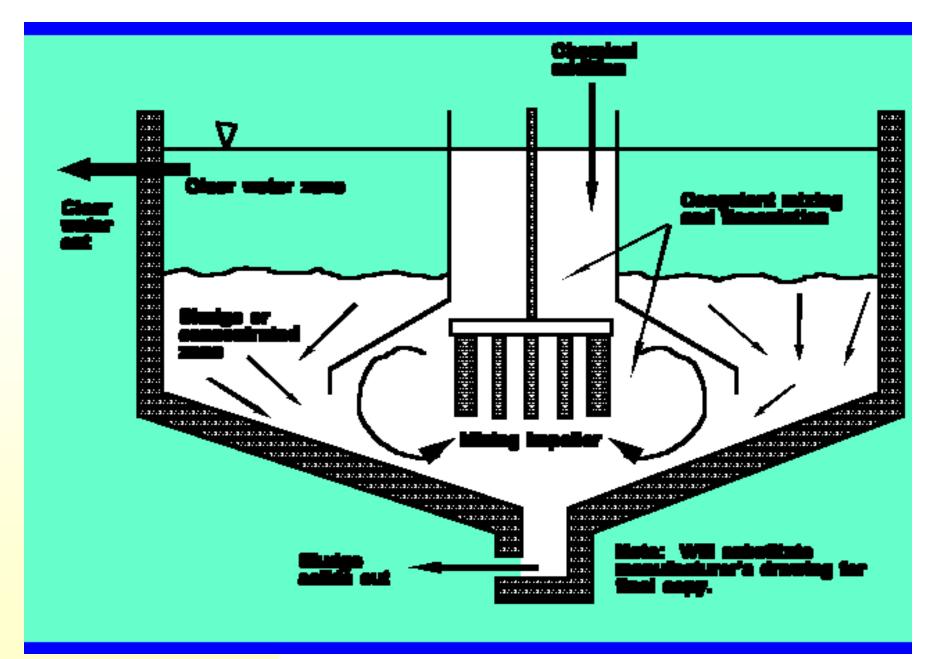
# Sedimentation Tank Configurations

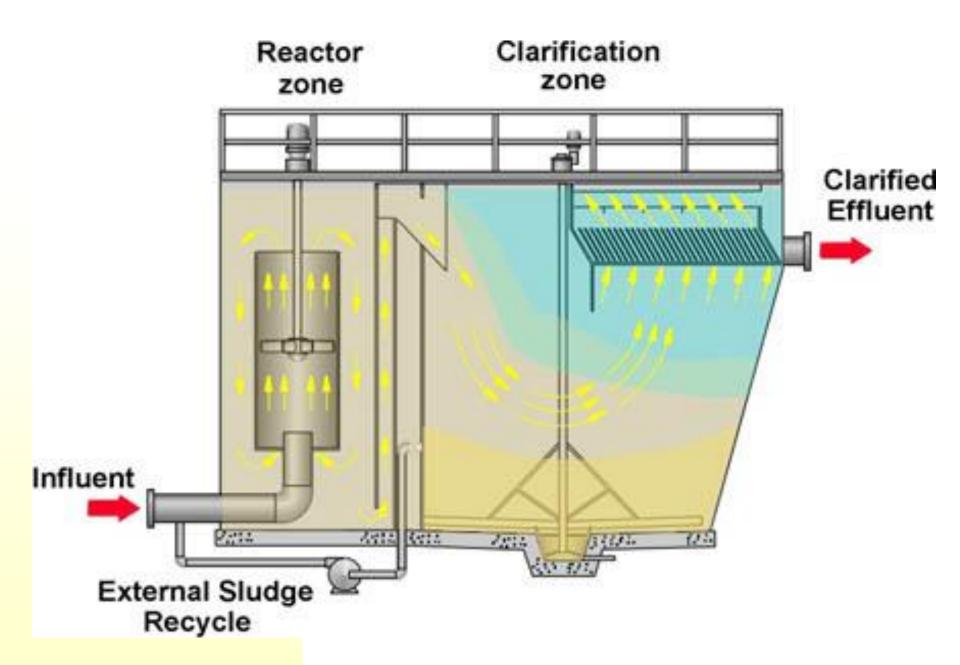
- Rectangular Clarifiers
  - most common
- Circular clarifiers
  - Center feed
  - Peripheral feed
- Flocculator-Clarifiers

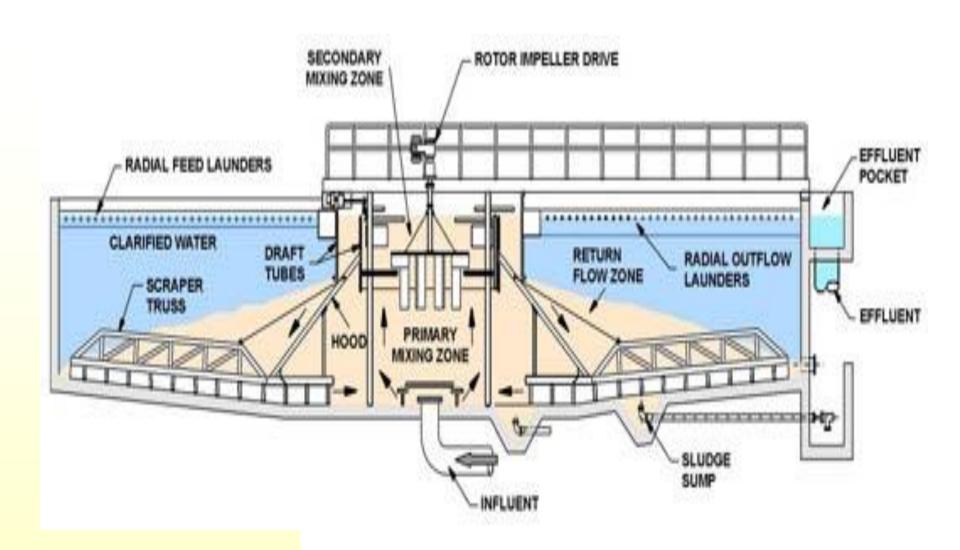


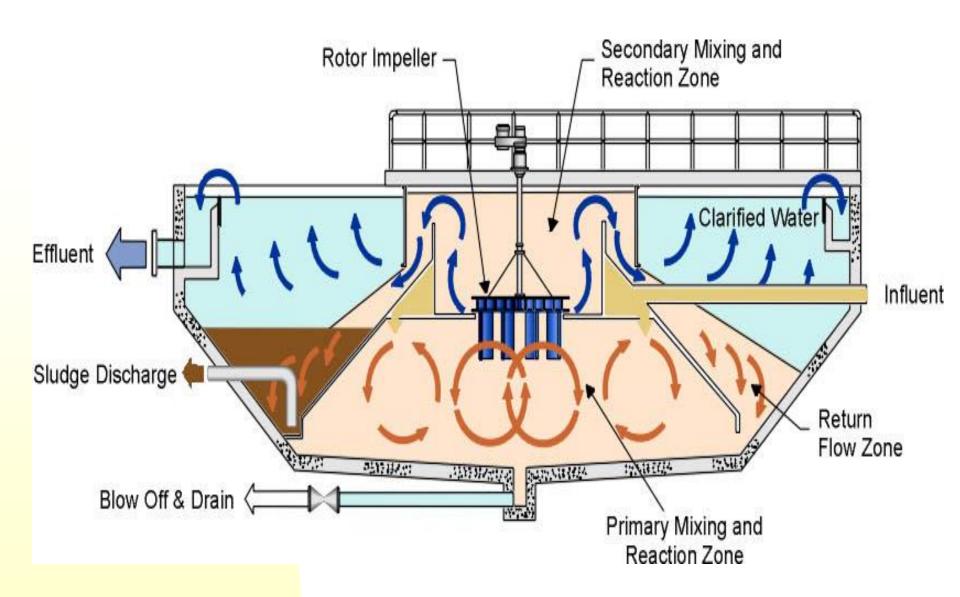
# Typical rectangular clarifier







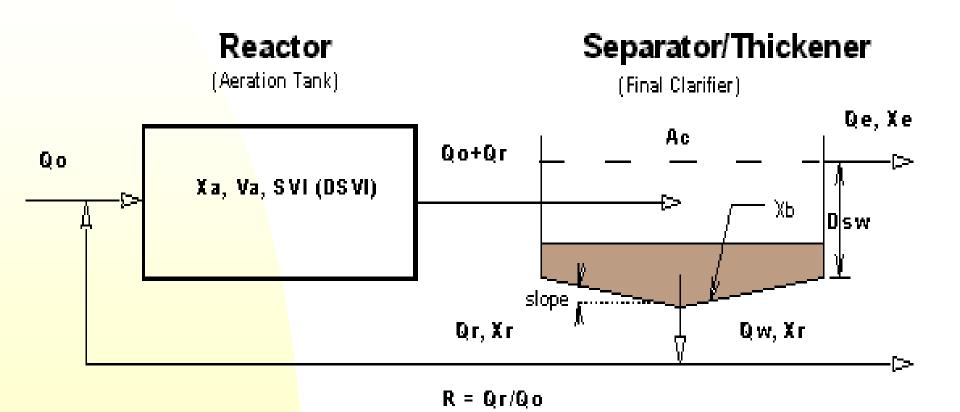








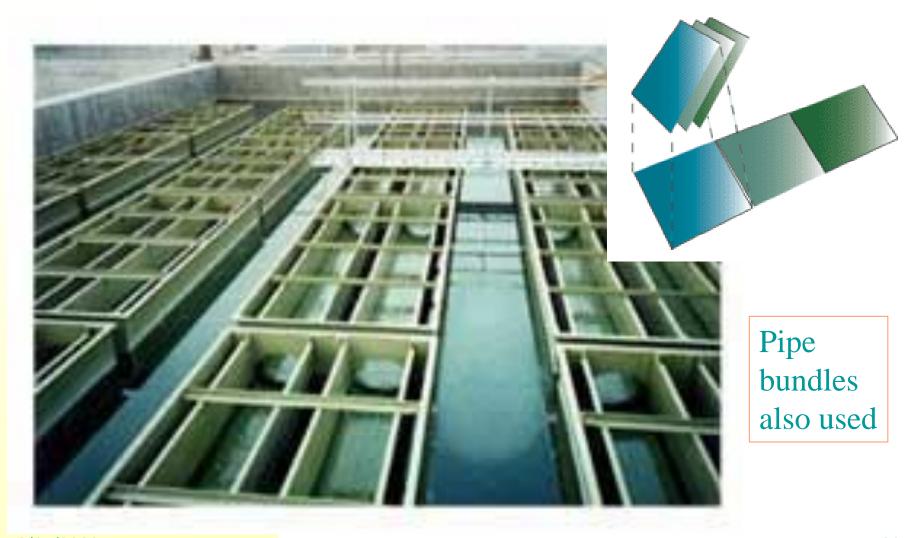
#### Activated Sludge Mass Balance over Settler





#### **Weir Details**

#### LAMELLA SETTLING TANKS: Shortening the settling distance

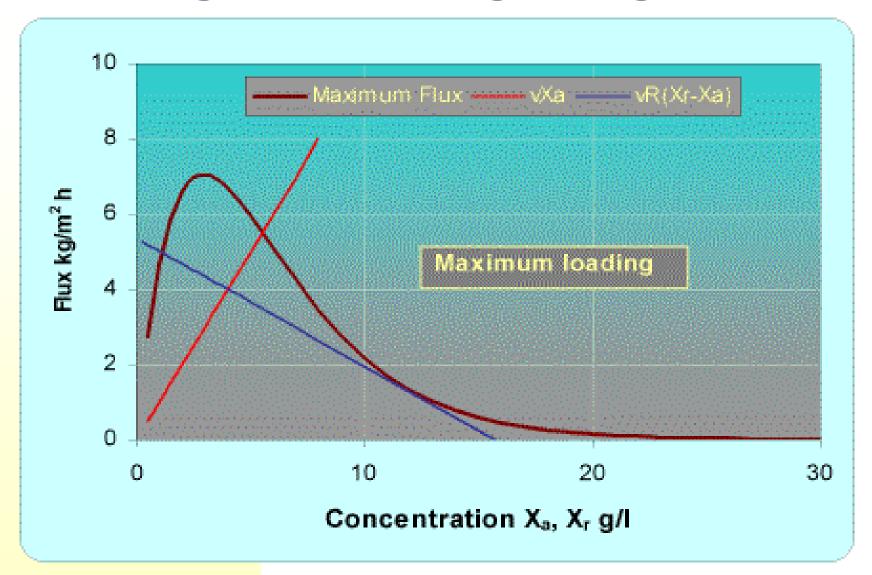


#### Sedimentation Tank Design

- Side water depth: about 12 ft.
- settling velocities: 2-6 ft/hr
- retention time: 4-8 h
- overflow rates:  $500-1000 \text{ gpd/ft}^2$  or  $0.3-0.7 \text{ gpm/ft}^2$  ( $20-40 \text{ m}^3\text{m}^{-2}\text{d}^{-1}$  or 0.8-1.7 m/h)
- linear velocities: less than 0.5 ft/min
   (2.5 mm/s) limits weir loading rate to
   100 200 m<sup>3</sup>m<sup>-1</sup>d<sup>-1</sup>



#### Sludge Thickening Design



#### **FLOTATION**

# Separation of low density flocs

If flocs have a density very close to that of water, it may be necessary to decrease their density by adding gas bubbles

#### **FLOTATION**

#### Separation of low density flocs

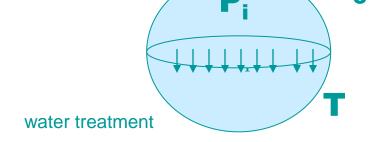
# Methods of forming gas bubbles

- Diffusion
- Vacuum
- Electrolysis
- Dissolved air

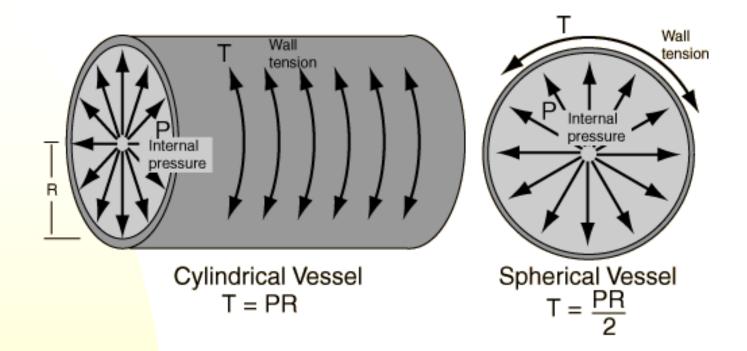
#### **Surface Tension and Bubbles**

- The <u>surface tension</u> of water provides the wall tension for the formation of bubbles. To minimize the wall tension the bubble pulls into a spherical shape (<u>LaPlace's law</u>).
- Pressure difference between the inside and outside of a bubble depends upon the surface tension and the radius of the bubble. Visualize the bubble as two hemispheres
- Note the internal pressure which tends to push the hemispheres apart is counteracted by the surface tension acting around the circumference of the circle.
- For a bubble with two surfaces providing tension, the pressure relationship is:

$$P_i - P_o = 4T/r$$



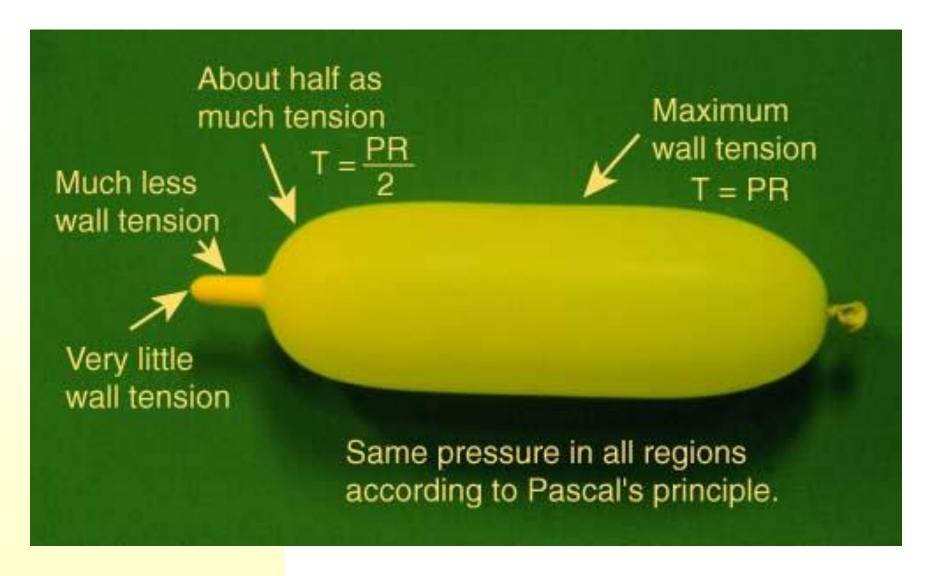
#### La Place's Law



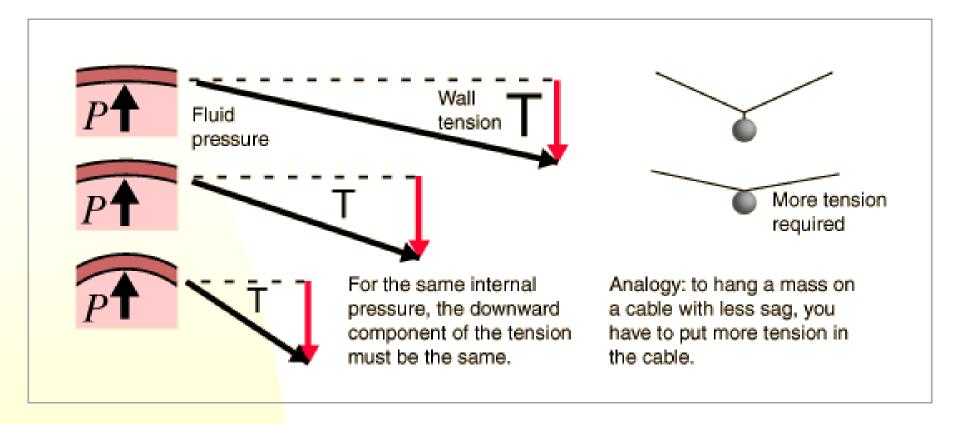
The larger the vessel radius, the larger the wall tension required to withstand a given internal fluid pressure.

For a given vessel radius and internal pressure, a spherical vessel will have half the wall tension of a cylindrical vessel.

#### **Wall Tension**



## Why does wall tension increase with radius?



If the upward part of the fluid pressure remains the same, then the downward component of the wall tension must remain the same. If the curvature is less, then the total tension must be greater in order to get that same downward component of tension.

#### **Bubble Pressure**

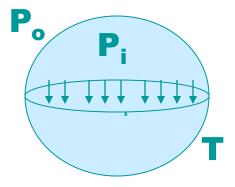
Net upward force on the top hemisphere of the bubble:  $F_{upward} = (P_i - P_o) \pi r^2$ 

The surface tension force downward around circle is twice the surface tension times the circumference, since two surfaces contribute to the force:

$$F_{\text{downward}} = 2T(2\pi r)$$

$$P_i - P_o = 4T/r$$
 for a spherical bubble

$$P_i - P_o = 2T/r$$
 for half a bubble



#### Attachment to floc

- Ratio of area/volume increases with decreasing size
- Forces acting on a gas bubble: Internal pressure x area
  - = surface tension x circumference
- Easier for bubble to form against solid

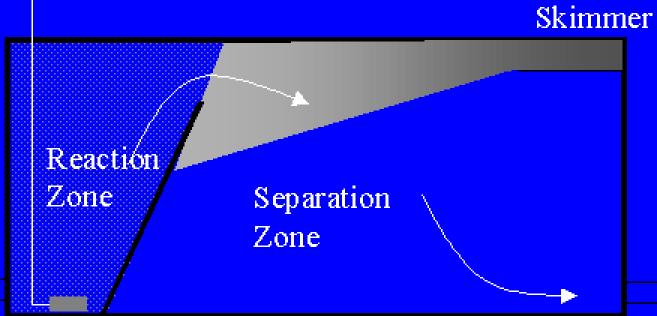
#### Dissolved Air Flotation (DAF)

- Alternative to Sedimentation
- Particles attach to air bubbles
- Best for removing low density floc
- Uses small tanks
  - high hydraulic loading (4-6 gpm/ft²)
  - low detention times ( $\sim$ 10 min)
- higher sludge solids conc.



# DAF Schematic

Dissolved Air From Saturator





#### Stokes's law for flotation

For Gravity Settling:

$$v_p = \frac{(\rho_p - \rho_w)d^2g}{18\mu}$$

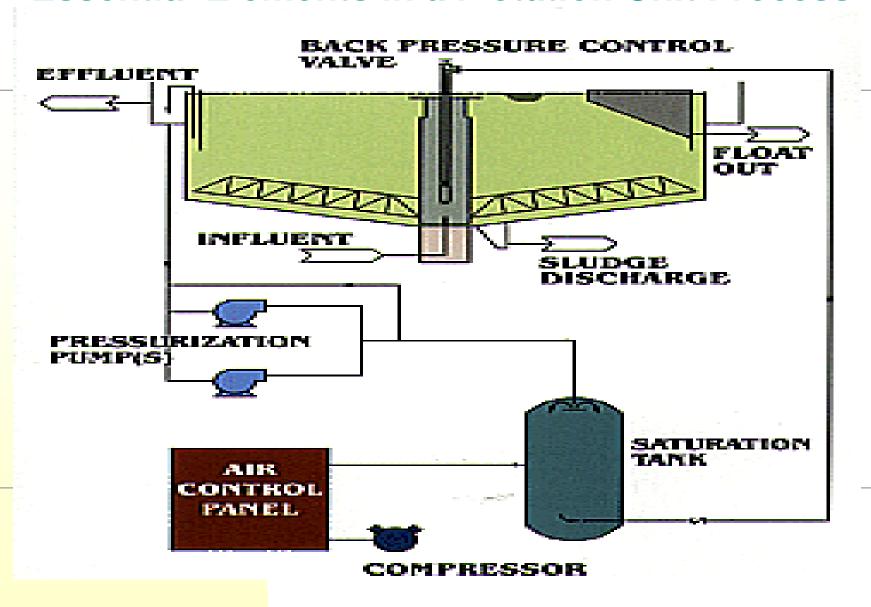
For DAF:

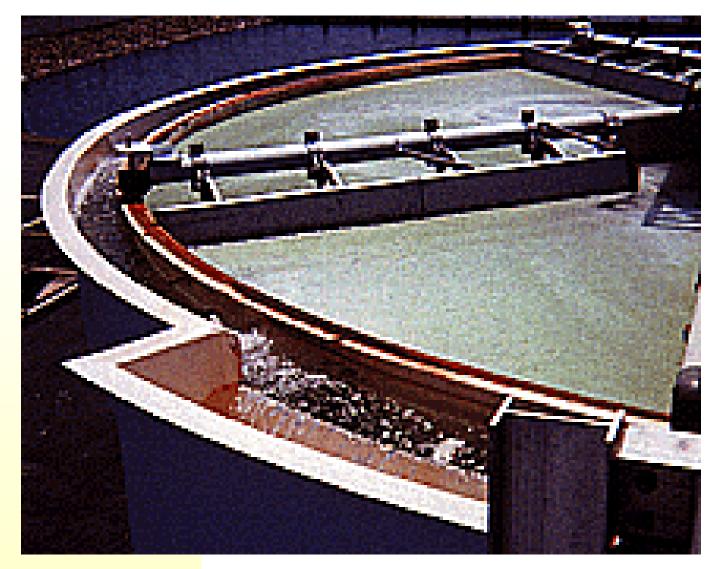
$$v_{pb} = \frac{(\rho_w - \rho_{pb})d_{pb}^2g}{18\mu}$$



Density and diameter of the Particle-bubble agglomerate ( $p_{pb}$  and  $d_{pb}$ ) are determined from simple geometry.

#### **Essential Elements in a Flotation Unit Process**





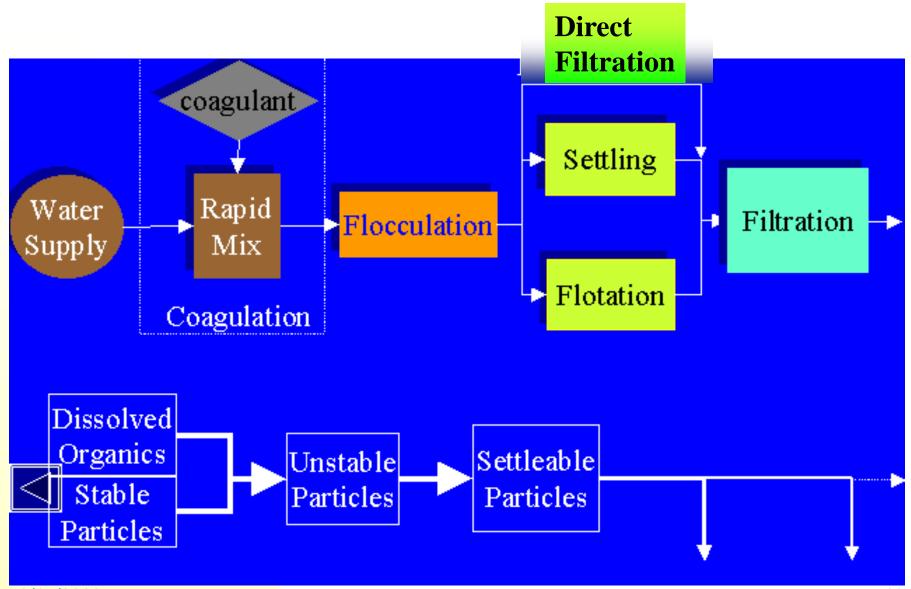
**Dissolved Air Flotation** 



#### Saturation tank for flotation



#### Overview of solid-liquid separation alternatives in water



# Softening

- Addition of:
  - Lime (Ca(OH)<sub>2</sub>)
  - Soda Ash (Na<sub>2</sub>CO<sub>3</sub>)
- Removes calcium and magnesium
- Removes particles
- Can also remove some DOC, but not as much as coagulation



Uses high pH

# Hardness Classification

Description of Hardness	Hardness, as mg CaCO₃/L
Soft	< 50
Medium	50 to 150
Hard	150 to 300
Extremely hard	> 300



# Softening Chemistry

#### <u>Stoichiometry</u>

$$Ca(OH)_2 + HCO_3^- + Ca^{+2} \rightarrow 2CaCO_3 \downarrow + 2H_2O$$

$$Mg^{+2} + Ca(OH)_2 \rightarrow Mg(OH)_2 \downarrow + Ca^{+2}$$

#### Therm odynamics

$$[Ca^{+2}][CO_3^{-2}] = 10^{-8.15}$$



$$[Mg^{+2}][OH]^2 = 10^{-9.2}$$

# What you need to be able to do

- Be able to size settling tanks on the basis of particle settling rates and identify important zones in the settling tank
- Be able to do a mass balance over a flotation unit to account for air usage
- Be able to size a flotation unit based on particle sizes and densities