

Islamic University of Gaza -Environmental Engineering Department

Water Treatment

EENV 4331

Lecture 4: Sedimentation

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4. Sedimentation in water Treatment

4.1 Definition of Sedimentation:

It is the process of removing solid particles heavier than water by gravity force.

- ☐ **Particles that will settle within a reasonable period of time can be removed using a sedimentation tank (also called clarifiers).**

- ☐ **Sedimentation is used in water treatment at the locations indicated in Figures 1 through 4.**

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4.2 Applications of sedimentation in water treatment:

1. Plain settling (or pre-sedimentation) of river surface water .
2. In filtration treatment plants treating surface water to removes flocculated solids. The sedimentation tank comes after the flocculation tank.
3. In Softening treatment plants treating hard water to removes flocculated solids. The sedimentation tank comes after the flocculation tank.
4. In aeration treatment plant removing iron and manganese from ground water

4. Sedimentation in water Treatment

4.3 Geometry of sedimentation tanks:

- ☐ Sedimentation tanks are either rectangular or circular tanks.
- ☐ Figures 5 to 10 show typical sedimentation tanks used in water treatment.

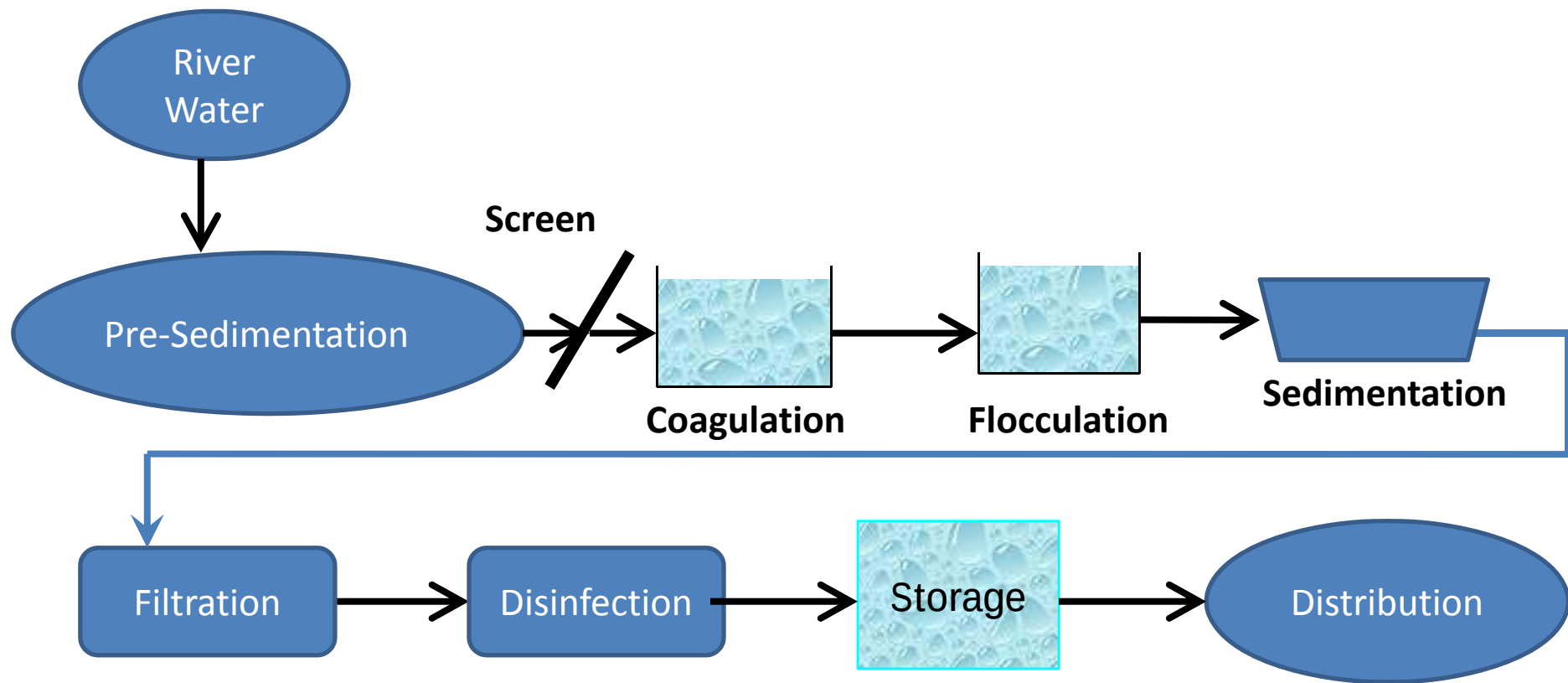


Figure 1: Filtration Treatment Plant (River Water)

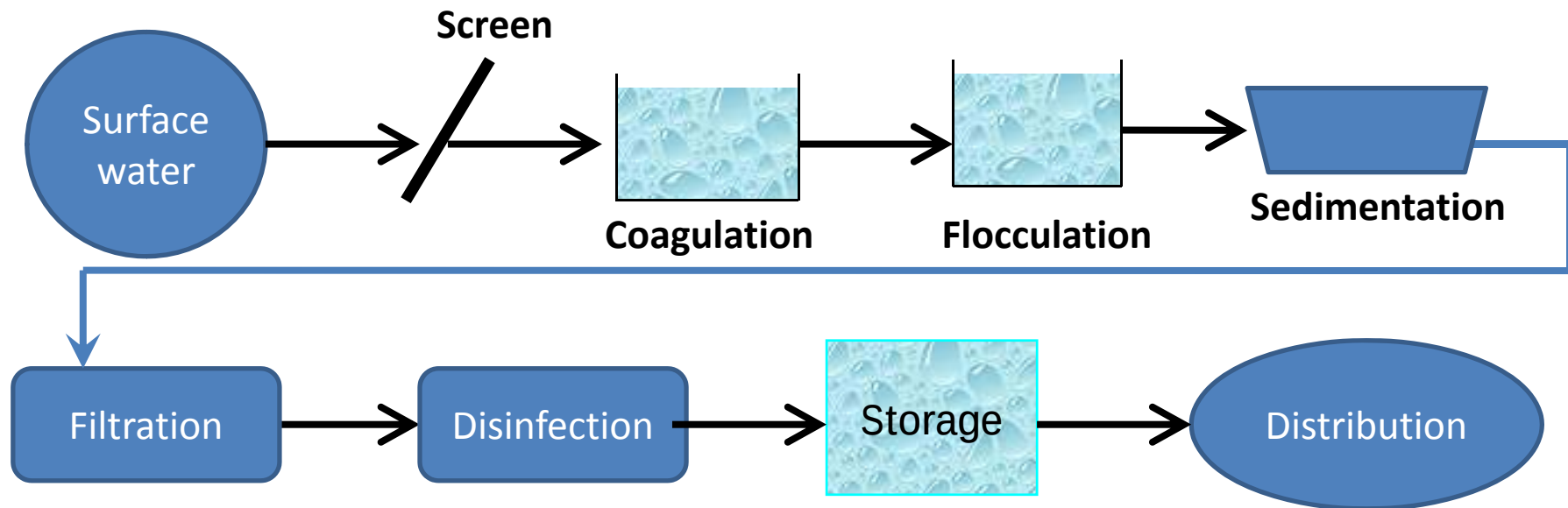


Figure 2 : Filtration Treatment Plant

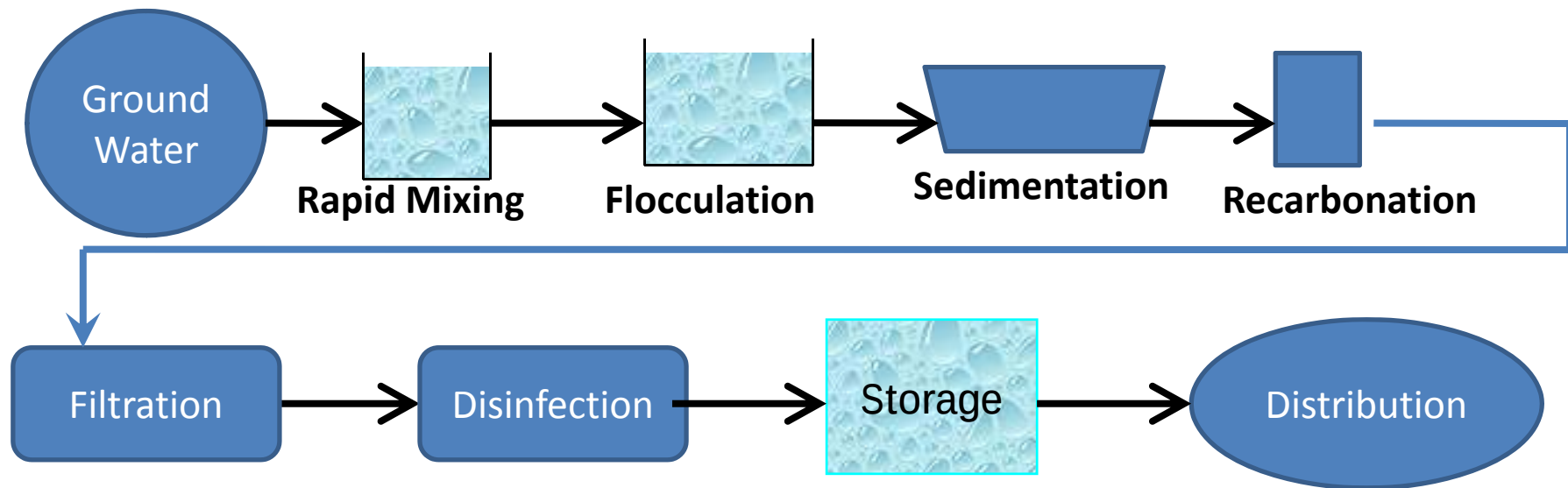


Figure 3: Softening Treatment Plant Single stage softening

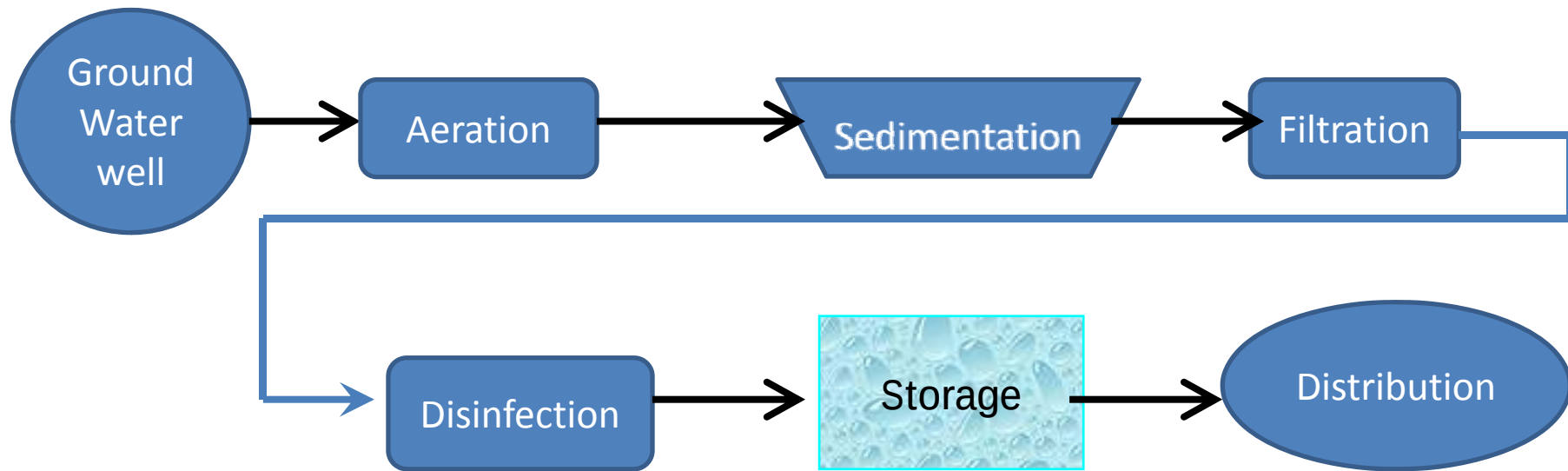


Figure 4 : Aeration Treatment Plant
(iron and manganese removal plant)



Figure 5 : Rectangular sedimentation Tank



Figure 6 : Rectangular sedimentation Tank



Figure 7 : Circular sedimentation Tank

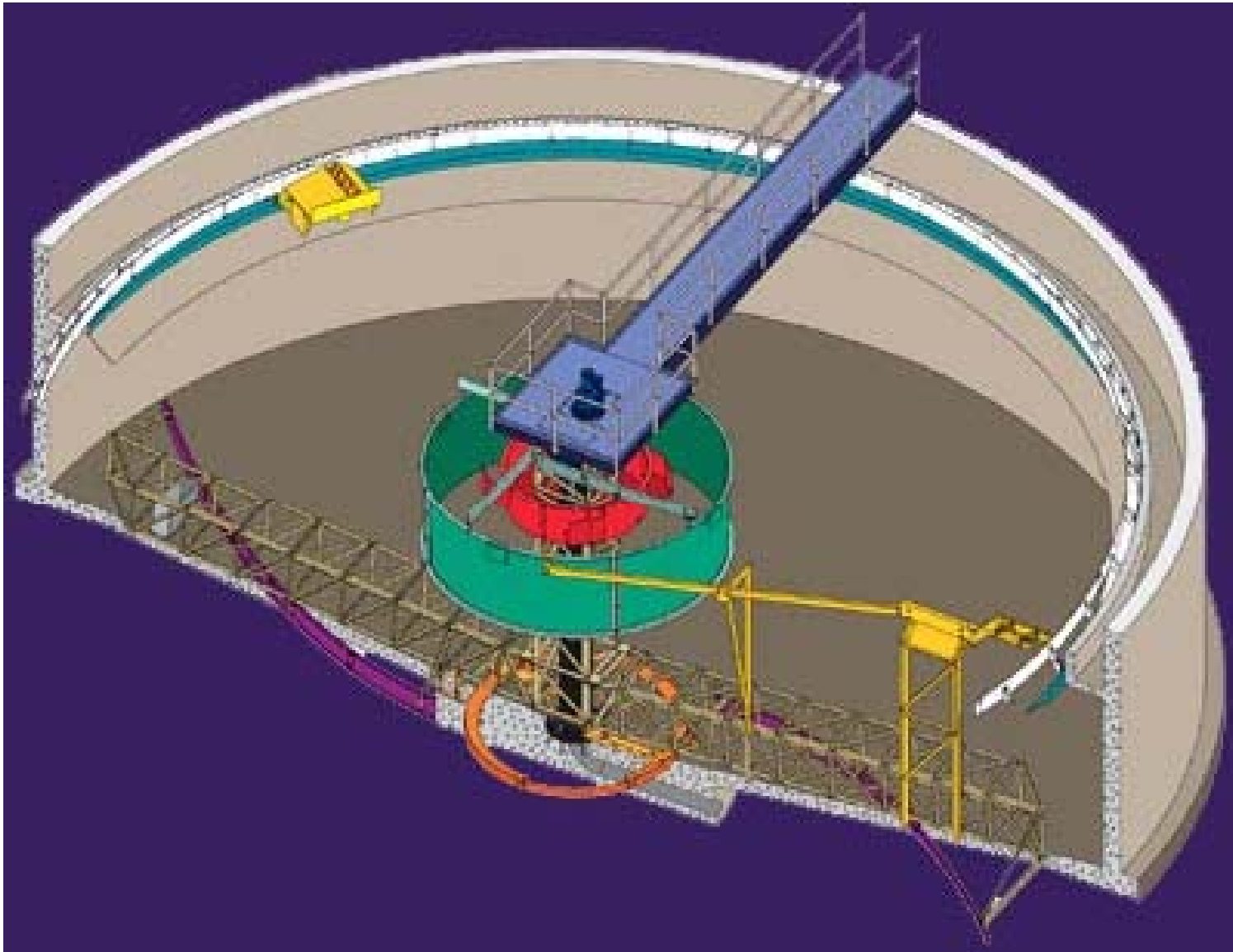
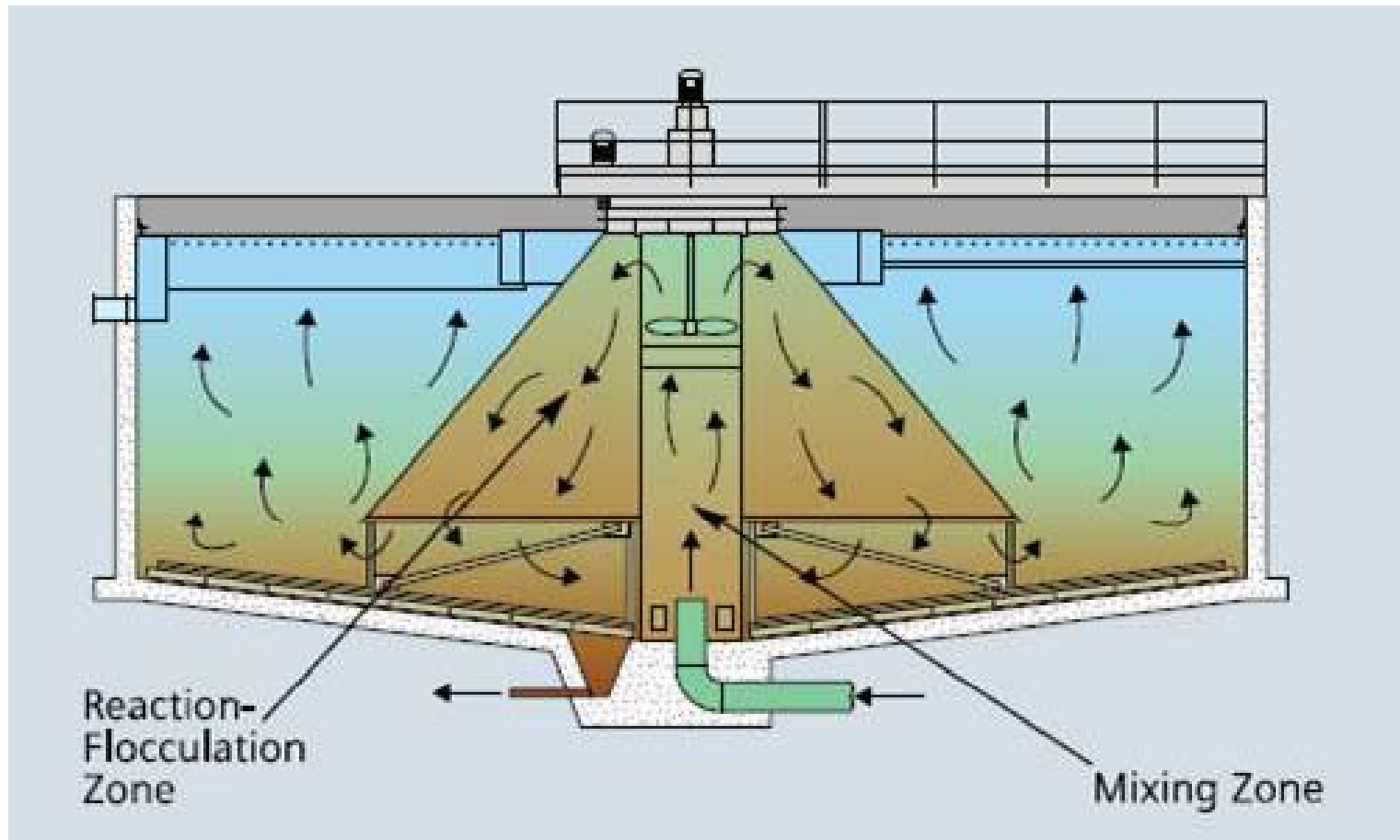


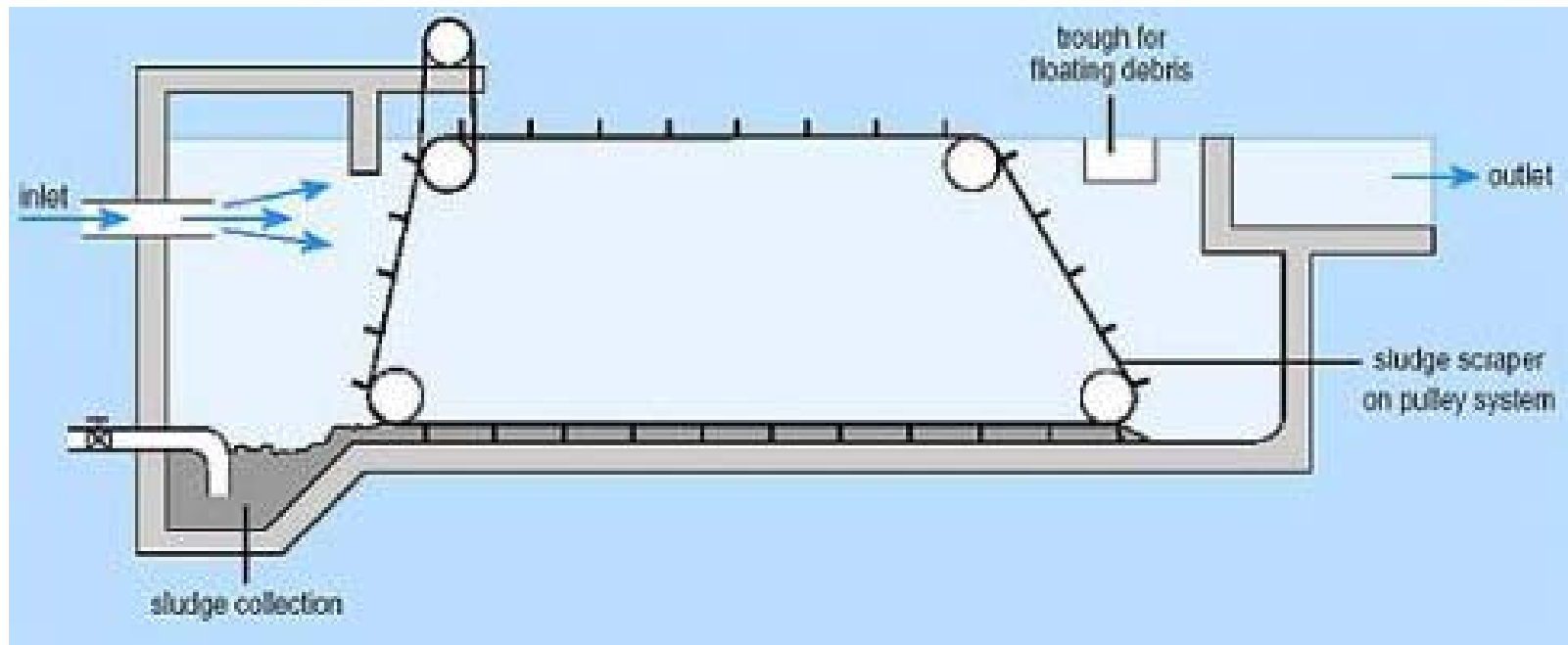
Figure 8 : Circular sedimentation Tank



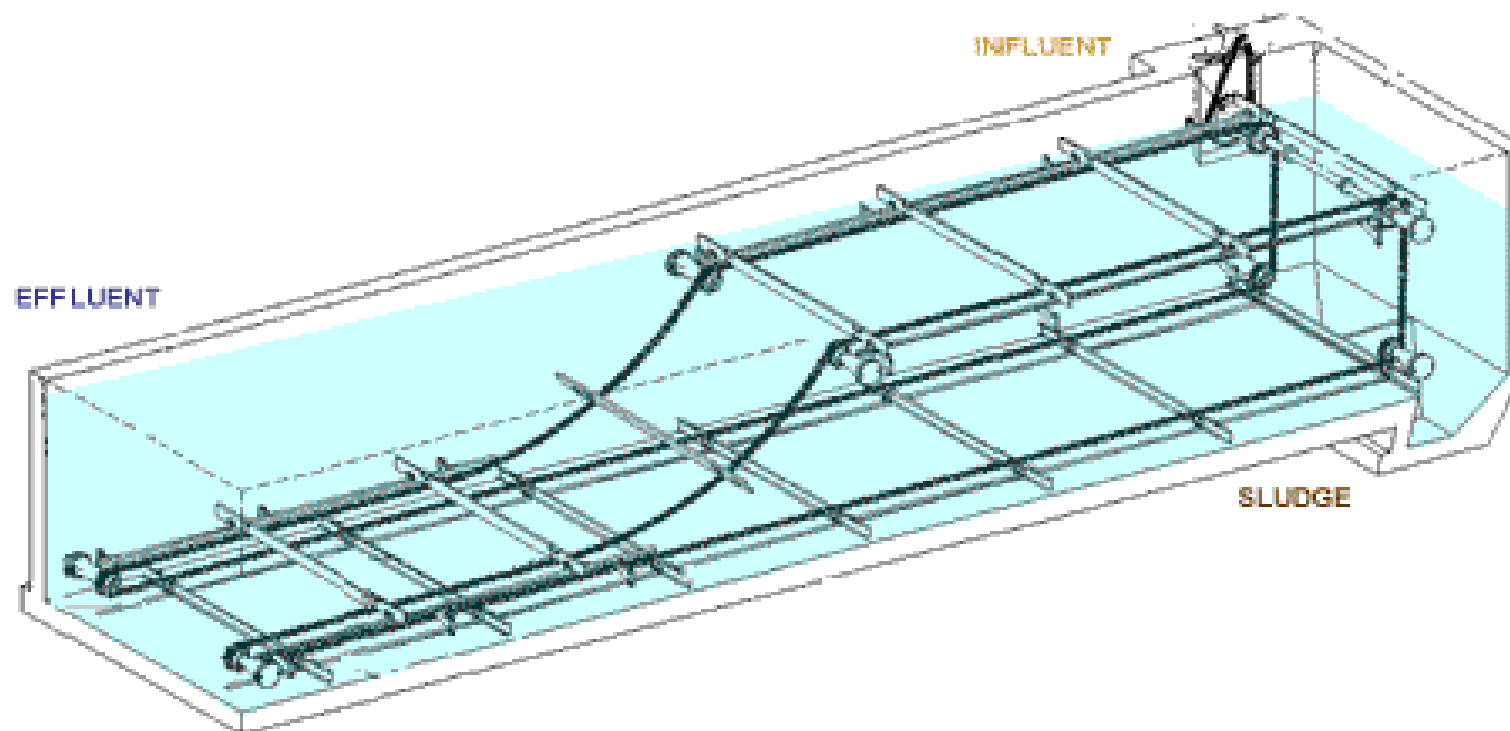
**Figure 9 : Circular sedimentation Tank
Solid contact type**



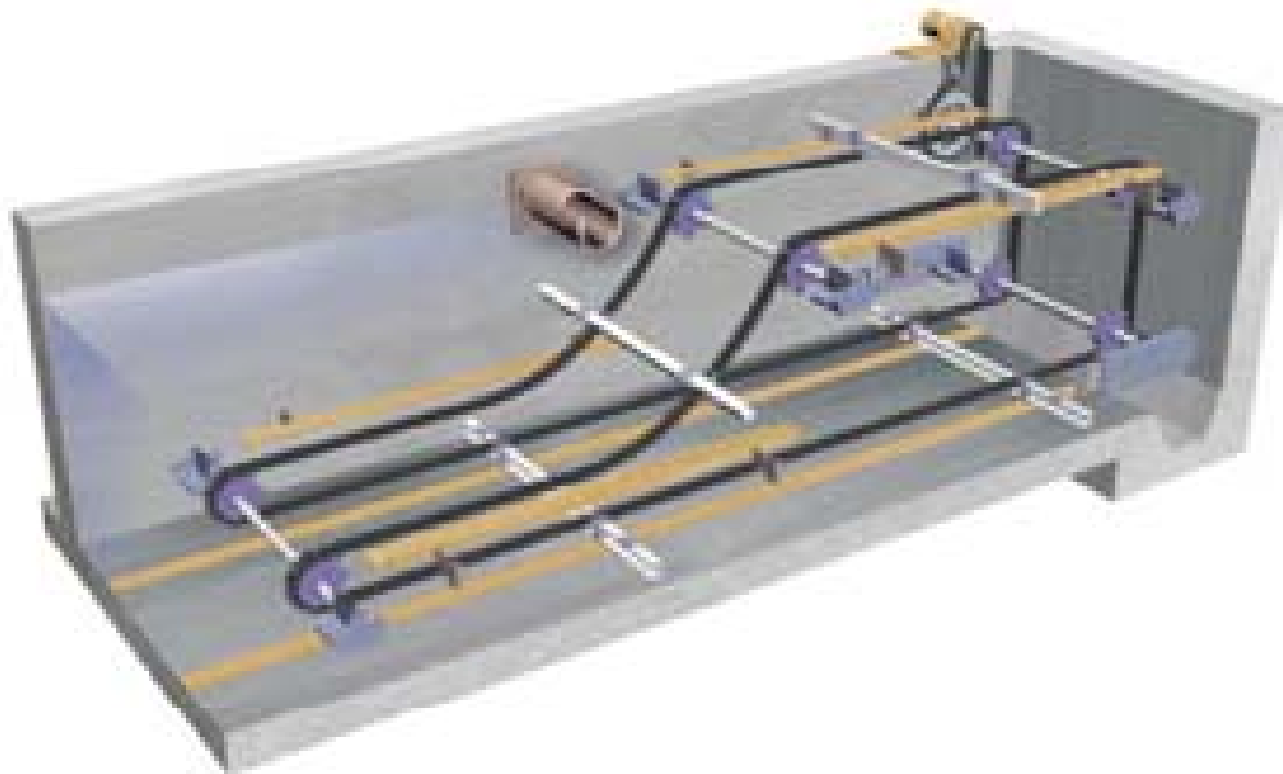
**Figure 10 : Circular sedimentation Tank
Solid contact type**



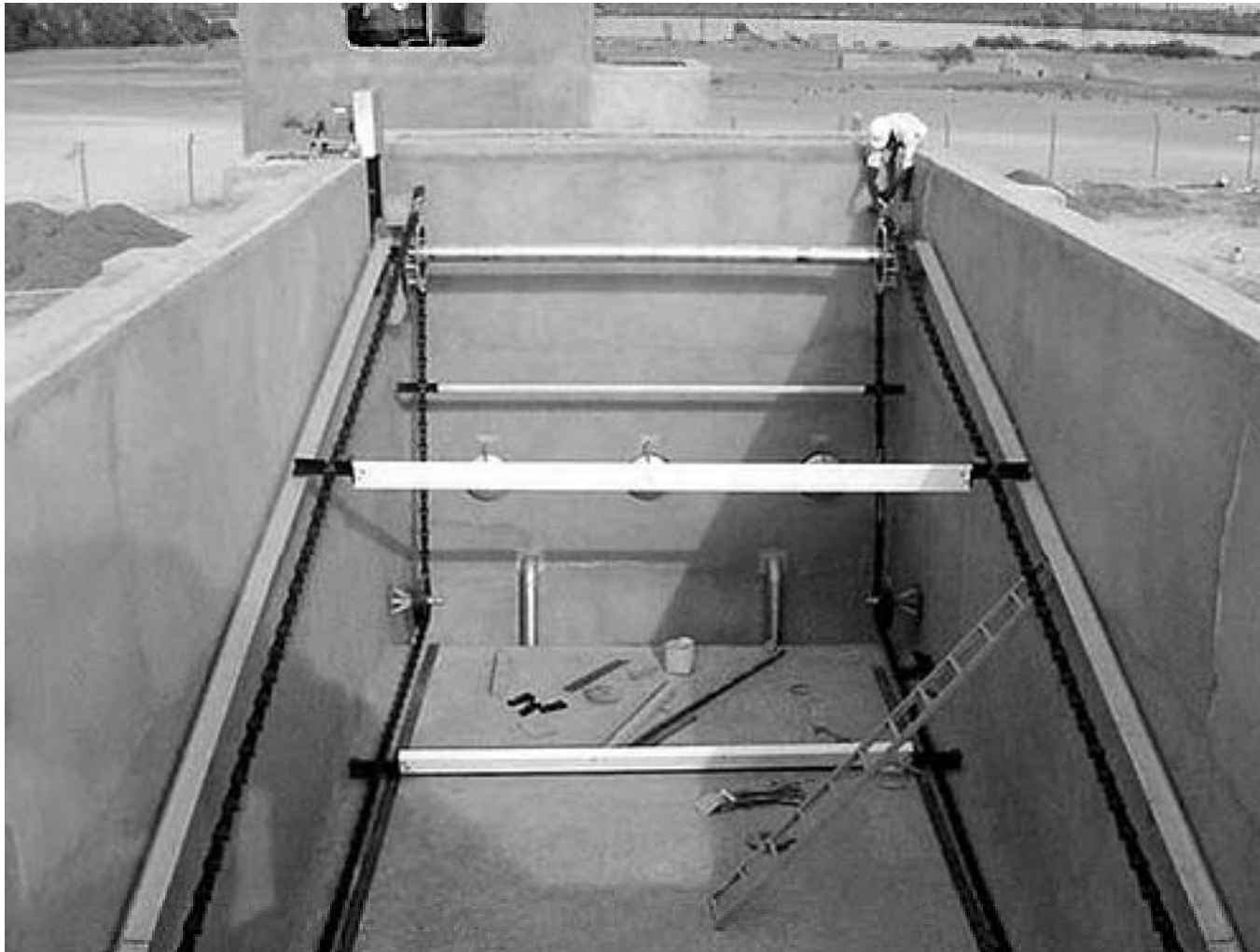
**Figure 11 : Rectangular sedimentation Tank
sludge collection system**



**Figure 12 : Rectangular sedimentation Tank
sludge collection system**



**Figure 13 : Rectangular sedimentation Tank
sludge collection system**



**Figure 14 : Rectangular sedimentation Tank
sludge collection system**

4. Sedimentation in water Treatment

4.3 Theoretical background on Sedimentation

4.3.1 Type of particles :

1) Discrete / individual particle

- Size, velocity constant during the settling
- Density 2,000 – 2,200 kg/m³

2) Flocculent particles

- Size, velocity fluctuates during the settling
- Particles flocculate and grow bigger in size
- Density 1,030 – 1,070 kg/m³

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4.3.2 Three classes of particles settling :

Type 1

- i) Particles settle discretely at a constant velocity
- ii) Settle as individual particles and do not flocculate.
- iii) E.g. : Sand, grit material
- iv) Occurs during :
 - i) Pre-sedimentation for sand removal
 - ii) Settling of sand during rapid sand filter cleaning
- v) Concentration : very low

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Type 2

- i) Flocculate during sedimentation
- ii) Size constantly changing
- iii) Settling velocity is changing
- iv) Settling velocity increase with depth and extent of flocculation.
- v) Occurs during :
 - i) Alum or iron coagulation
- vi) Concentration : low

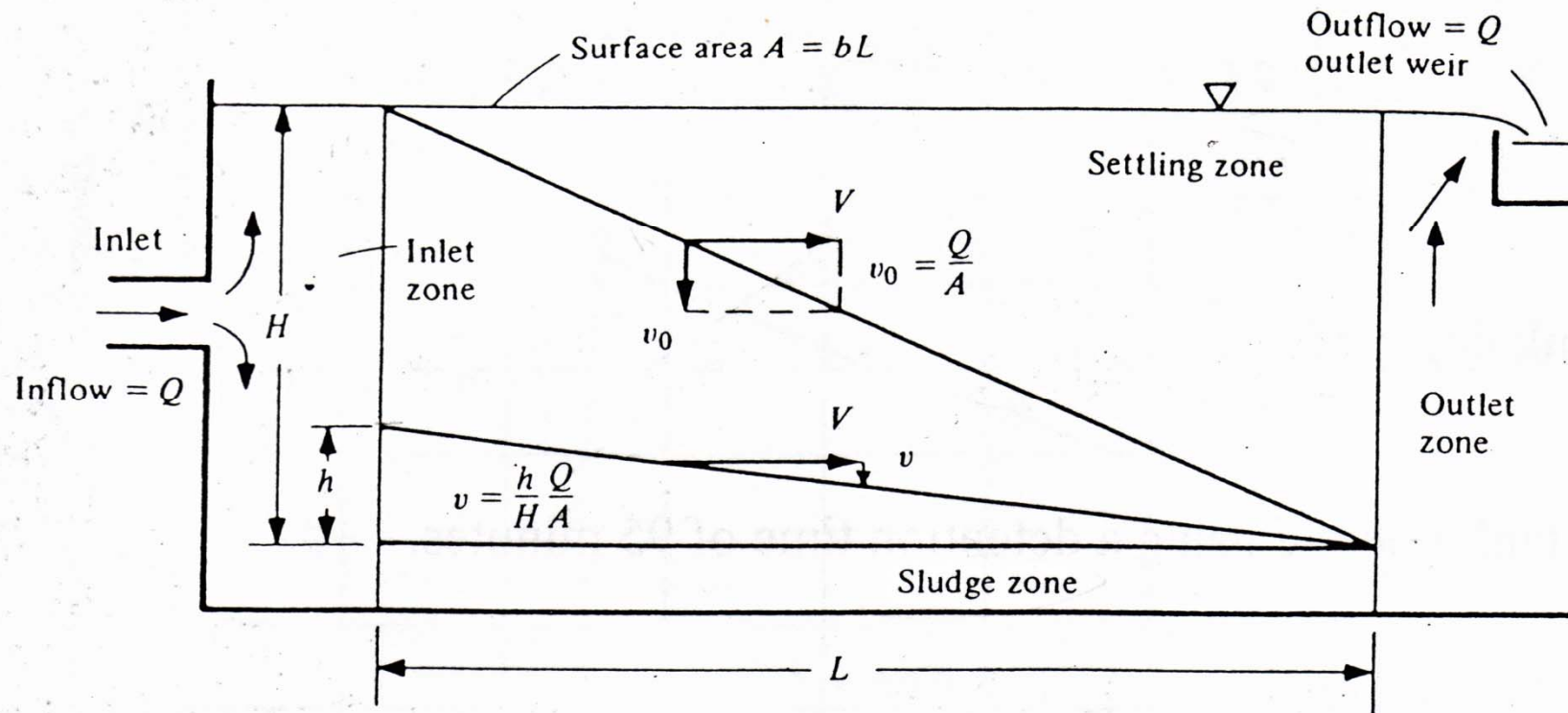
4. Sedimentation in water Treatment

Type 3 or Zone

- i) Settle as mass and form a layer – “blanket
- ii) Concentration high (greater than 1000 mg/L)
- iii) Distinct clear zone and sludge zone are present.
- iv) Occurs during :
 - i) Lime-softening sedimentation
 - ii) Sludge thickeners in water treatment.

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4.4 Sedimentation theory



An ideal rectangular sedimentation tank illustrating the settling of discrete particles.

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- Settling velocity (v_s) must be determined to assure good sedimentation tank design.
- Overflow rate (v_o) must be set at some value LESS THAN or EQUAL to V_s

$$v_s = \frac{H}{t}$$

$$v_s = \frac{H}{t} = \frac{H}{\left[\frac{V}{Q} \right]} = \frac{HQ}{l * W * H} = \frac{Q}{A_s}$$

But

$$v_o = \frac{Q}{A_s}$$

So

$$v_o = v_s$$

Where

- Q = flow rate (m³/h)
A_s = surface area (m²)
H = depth of water, m
W = tank width, m
L = tank length, m
t = detention time, hr

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4.5 Design of Sedimentation tanks

4.5.1 Plain Sedimentation:

Particles settle separately:

$$V_s = \sqrt{\frac{4g(\rho_s - \rho)d}{3C_D\rho}}$$

V_s = settling velocity

D = particle diameter

ρ = water density

ρ_s = particle density

C_D = drag coefficients

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4.5.1 Plain Sedimentation:

Drag coefficient is calculated as:

$R_e < 1$, Laminar Flow $\rightarrow$

$$C_D = \frac{24}{R}$$

$1 < R_e < 10^4$, Transitional Flow $\rightarrow$

$$C_D = \frac{24}{R} + \frac{3}{\sqrt{R}} + 0.34$$

$R_e > 10^4$, Turbulent Flow $\rightarrow$

Where R = Reynolds number

$$C_D = 0.40$$

μ = dynamic viscosity, N.s/m²

$$R = \frac{\rho V_s D}{\mu}$$

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4.5 Design of Sedimentation tanks

4.5.1 Plain Sedimentation:

At laminar flow, settling velocity equation is simplified to Stocks law:

$$v_s = \frac{g(\rho_s - \rho)D^2}{18\mu}$$

V_s = settling velocity

D = particle diameter

ρ = water density

ρ_s = particle density

C_D = drag coefficients

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Example 4.1 :

Find the settling velocity (v_s) for sand particles with a diameter of 0.020mm.

$\rho = 2650 \text{ kg/m}^3$, $\mu = 1.002 \times 10^{-3} \text{ N.s/m}^2$ at 20°C , $\beta = 0.05$, $f = 0.03$. what is v_s for particles with $D = 0.5 \text{ mm}$?

Solution:

Assume first the flow is laminar and check for Reynolds number:

$$v_s = \frac{9.80(2650 - 1000)(0.02 \times 10^{-3})^2}{18 * 1.002 * 10^{-3}} = 3.59 \times 10^{-4} \text{ m/s}$$

$$R = \frac{\rho V_s D}{\mu} = \frac{1000 * 3.58 * 10^{-4} * 0.20 * 10^{-3}}{1.002 * 10^{-3}} = 0.00715$$

→ $R < 1$, so its laminar flow

For particles with $D = 0.5\text{mm}$:

$$v_s = \frac{9.81(2650 - 1000)(0.5 \times 10^{-3})^2}{18 * 1.002 * 10^{-3}} = 0.22 \text{ m/s}$$

$$R = \frac{\rho V_s D}{\mu} = \frac{1000 * 0.22 * 0.50 * 10^{-3}}{1.002 * 10^{-3}} = 110$$

→ $R > 1$, so its transitional flow

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so →

$$C_D = \frac{24}{110} + \frac{3}{\sqrt{110}} + 0.34 = 0.84$$

$$v_s = \sqrt{\frac{4 * 9.81 (2650 - 1000) 0.5 * 10^{-3}}{3 * 110 * 1000}} = 0.11 \text{ m/s}$$

Solve again for R_e : →

$$R_e = 55$$

→

$R > 1$, so its transitional flow
O.K

Solve again fir C_D : →

$$C_D = 1.18$$

Solve again for v_s : →

$$v_s = 0.10 \text{ m/s}$$

$$\text{Take } v_0 = v_s = 3.59 * 10^{-4} \text{ m/s} = 31 \text{ m/d} = 31 \text{ m}^3 / \text{m}^2 . \text{d}$$

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4.5 Design tanks

4.5.1 Plain Sedimentation:

Example 4.2:

Design pre-sedimentation tanks to be used to remove grit and sand from a river water that is used to produce 20000 m³/d drinking water .Use the overflow rate and horizontal velocities calculated in example 4.1. Use two tanks.

Solution:

$$\text{Take } v_0 = v_s = 31 \text{ m}^3 / \text{m}^2 \cdot \text{d}$$



$$v_0 = \frac{Q}{A_s} = \frac{Q}{W * l}$$

*Flow/tank = (Q/2)= 20000/2 = 10000 m³/dh

As = 10000/31 = 322.5 m²

•Select Width to length ratio 1:4

•A = W* 4W = 322.5 m²  W= 8.98 m , L = 35.92 (take W= 9 m, L= 36 m)

•Assume detention time = 3 hrs

$$H = t * V_0 = (3 * 31) / 24 = 3.88 \text{ m} \approx 3.90 \text{ m}$$

•V_h = Q/(W*H) = 10000/(24*60*9*3.9) = 0.198 m/min

•Take weir loading rate = 250 m³/m.d:

L_{weir} = Q/W_{load} = 10000/250 = 40 m , Use suspended troughs inside the tank.

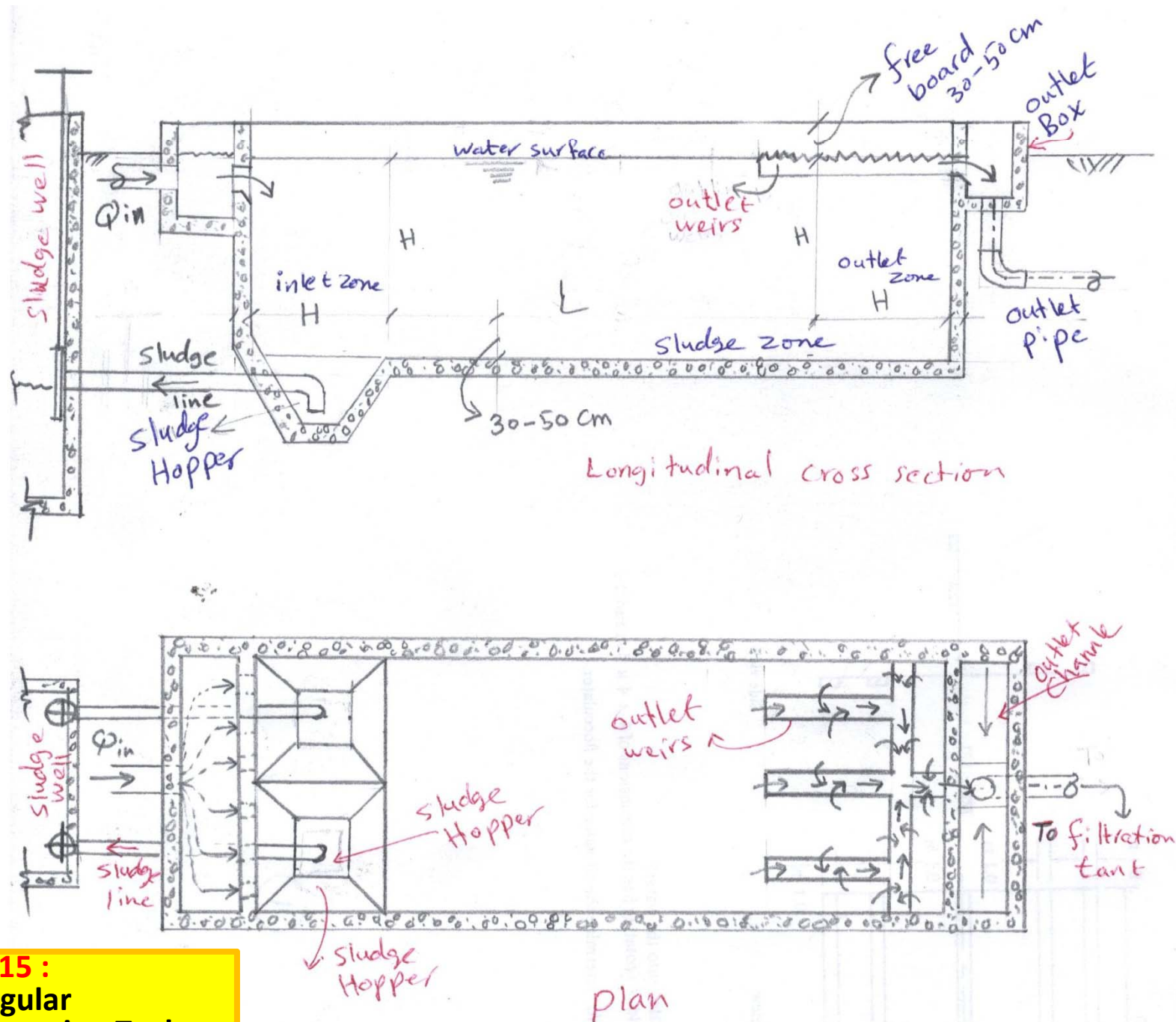


Figure 15 :
Rectangular
sedimentation Tank

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Example 4.3:

Repeat example 4.3 using circular tank.

Note: the maximum tank diameter is 40 m

Solution:

$$\text{Take } v_0 = v_s = 31 \text{ m}^3 / \text{m}^2 \cdot \text{d} \longrightarrow v_0 = \frac{Q}{A_s}$$

*Flow/tank = $(Q/2) = 20000/2 = 10000 \text{ m}^3/\text{d}$

$A_s = 10000/31 = 322.5 \text{ m}^2$

• $A_s = \pi D^2/4 = 322.5 \text{ m}^2$ $D = 20.27 \text{ m} \approx 20.30 \text{ m} < 40 \text{ m}$

• Assume detention time = 3 hrs

$H = t \cdot V_0 = (3 \cdot 31)/24 = 3.88 \text{ m} \approx 3.90 \text{ m}$

Check horizontal velocity at the beginning and end of settling zones:

• $V_h = Q/(\pi D_{in} H) = 10000/(24 \cdot 60 \cdot 3.14 \cdot 3.9 \cdot 3.9) = 0.145 \text{ m/min}$ (End of inlet zone)

• $V_h = Q/(\pi D_{out} H) = 10000/(24 \cdot 60 \cdot 3.14 \cdot 20.3 \cdot 3.9) = 0.024 \text{ m/min}$ (beginning of outlet zone)

• Take weir loading rate = $250 \text{ m}^3/\text{m} \cdot \text{d}$:

$L_{weir} = Q/W_{load} = 10000/250 = 40 \text{ m}$, Use suspended troughs inside the tank.

Available Length = $\pi D_{total} = \pi(2H + D) = 3.14 \cdot (2 \cdot 3.9 + 20.30) = 88.23 \text{ m} > 40 \text{ m}$ O.K

Available $W_{load} = Q/L = 10000/88.23 = 113.34 \text{ m}^3/\text{m} \cdot \text{d} < 250 \text{ m}^3/\text{m} \cdot \text{d}$ O.K

H = side wall height (tank depth)

$D_{in} = H$

$D_{out} = H + D$

$D_{total} = 3H + D$

D = diameter calculated from
the Over flow rate

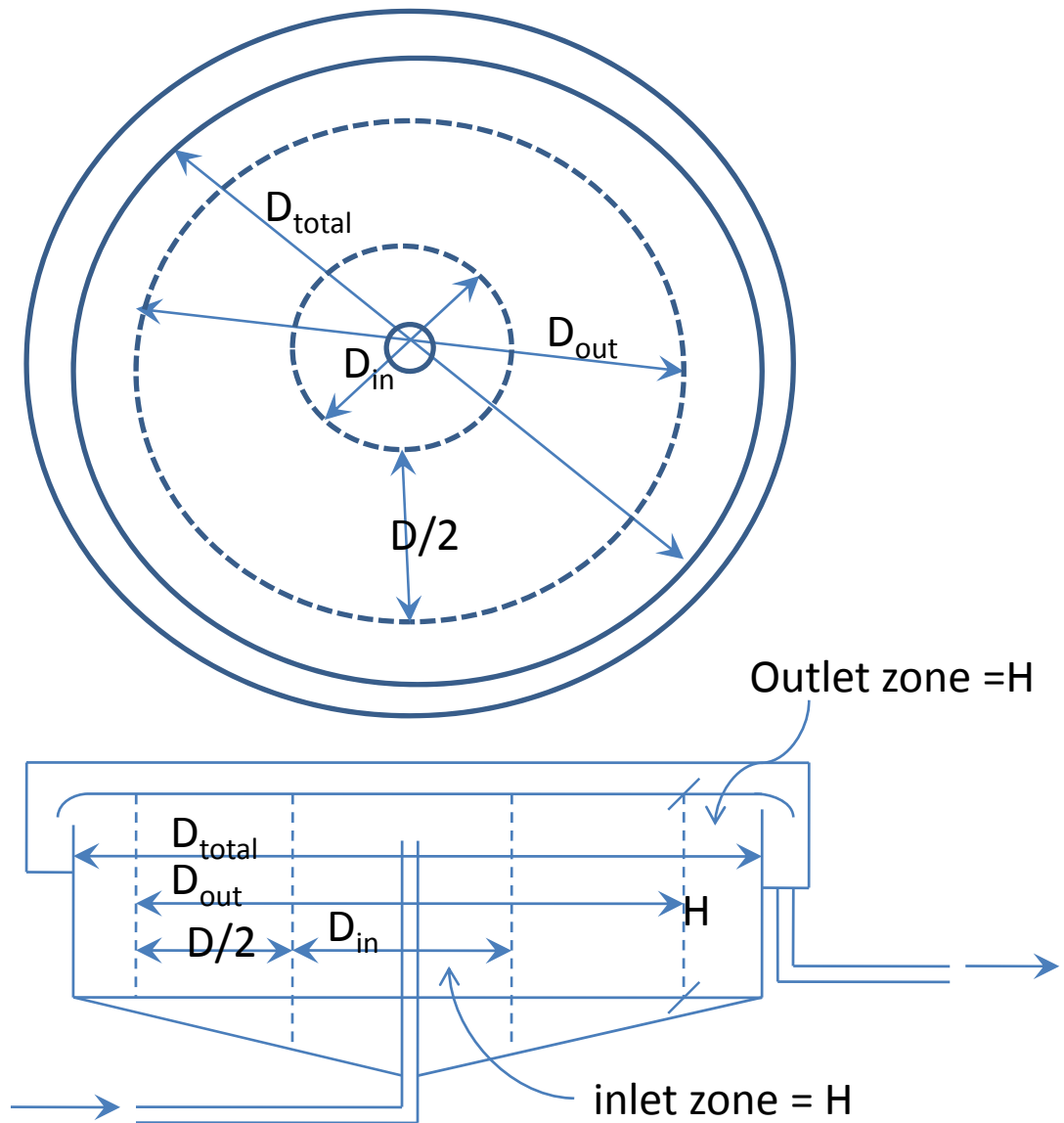


Figure 16 :
Circular
sedimentation Tank
Dimensions definition

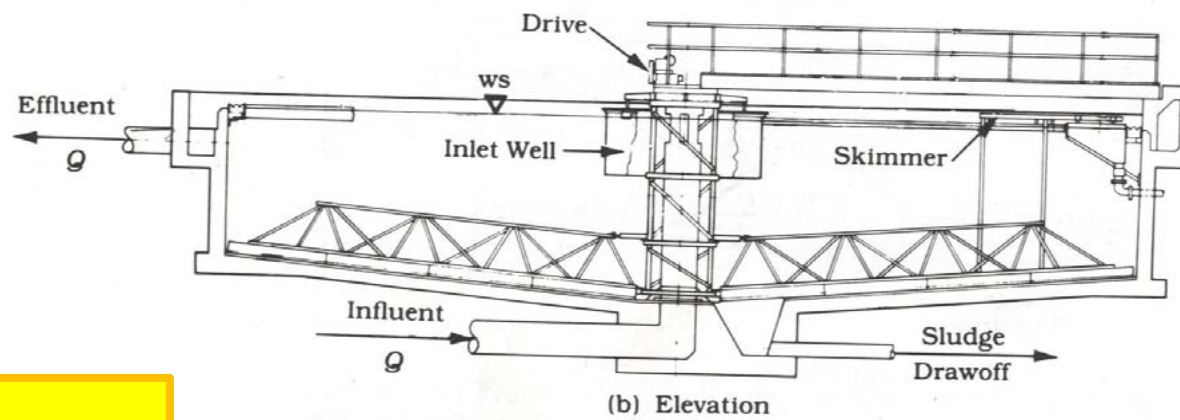
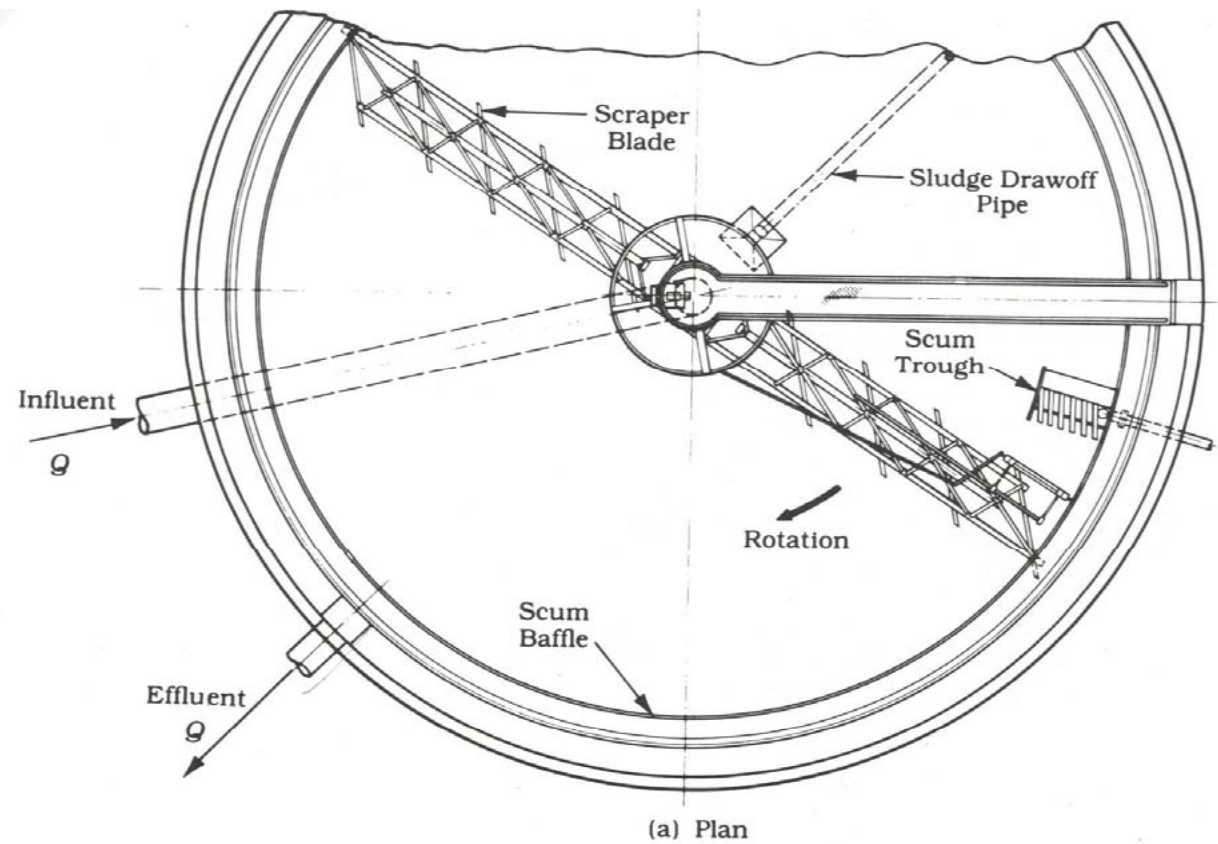


Figure 17 :
Circular
sedimentation Tank

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4.5 Design of Sedimentation tanks

4.5.2 Flocculent Sedimentation (type 2 and 3):

The design procedure for sedimentation tanks of type 2 and 3 are the same as type 1. The difference is mainly in the overflow rate (v_0) . The following table gives the design criteria of these two types.

Process	Settling type	Detention time (h)	Surface loading rate ($\text{m}^3/\text{m}^2.\text{d}$)	Weir loading rate ($\text{m}^3/\text{m}.\text{d}$)
Coagulation	2	4-8	20-40	250
softening	3	2-6	40-60	250