

WATER QUALITY SOLUTIONS SWRO Pretreatment

by

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Global Product Manager, Desalination





1924 - F.B. Leopold Establishes Company

1942 - F.O. Leopold Moves Company to Zelienople, PA

Company sold by Leopold family in 1972

2004 – Leopold celebrated 80th Anniversary

June 2006 – ITT Acquires Leopold

November 2011, ITT changes name to Xylem

Leopold Headquarters: Zelienople, PA, USA

Zelienople, PA – Products Manufacturing:

Ontario, Canada - Products

Watsontown, PA - Anthracite

Zelienople, PA – Americas United Kingdom – EU Sales Offices:

Dubai, UAE – Middle East

Singapore – Asia Pacific



Capabilities

Extensive Experience
Over 9,000 installations worldwide
Full Engineering Design Services
Computational Fluid Dynamics (CFD) Analysis
Research & Development (PDC)
Field Services
Variety of Pilot Facilities
DAF, Filtration, Denitrification, Desalination PT
Gold Tag Service





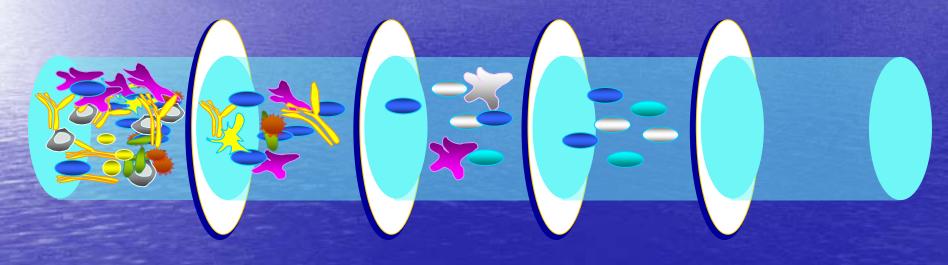
The Desalination Process



Microfiltration >0.1 μm

Ultrafiltration 0.1-0.01µm Nanofiltration 0.01-0.001µm **Reverse Osmosis**

< 0.001µm

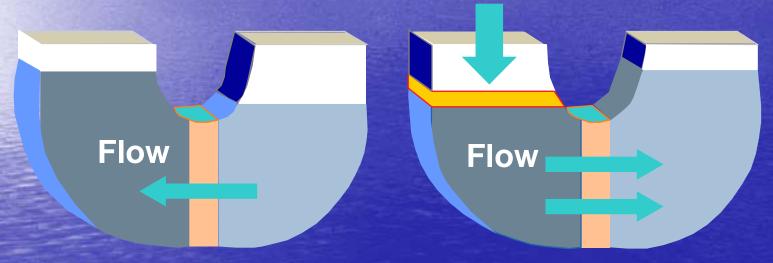




Reverse **Osmosis**

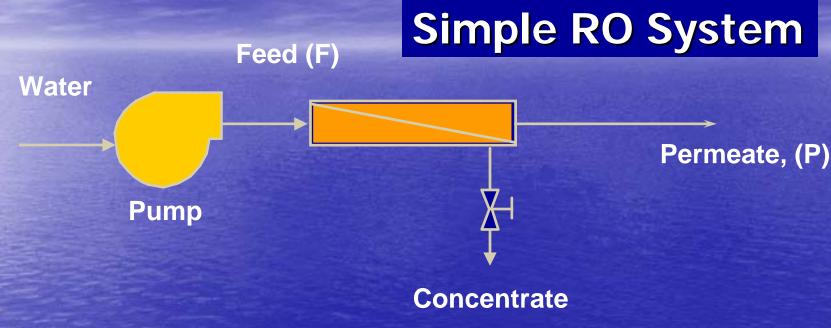
Osmosis

Applied Pressure



- **Concentrated** Solution
- Membrane Dilute Solution





Recovery Rate = P flow/F flow
Salt Rejection = 1-(P tds/F tds)
Pressure Drop = F pressure- C pressure



Facts: RO Membranes

- Pore Size of 0.0005 micron
- Removes Salt & Soluble ions
 - Low Flux rate: 10-30 GFD
- Concentrate multiplies problem
- Permeate usually not degraded by poor feed water
 - Low Recovery Rate: 30-40%
 - High pressure: 55-76 bar
 - Fails due to inadequate pretreatment



Membrane Fouling

Physical

- Deposits/entrapped particles on surface and into membrane pores

Biological

- Colonies which grow into slime deposits in feed spacer



Poor or no pre-treatment can result in Lower Recovery Rates

Higher waste volumes to handle Less finished water to provide customer

Lower Flux Rates

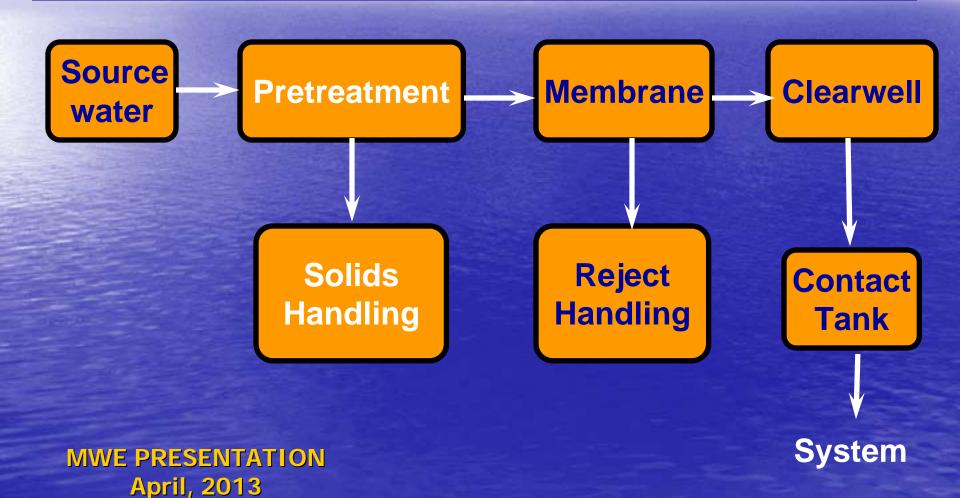
Higher capital costs for additional membranes Larger foot print for treatment facility

Increased Operational Cost

Increased pressure - higher energy cost
Requires more cleaning – more chemicals
Reduces membrane life – capital replacement



Ideal Membrane Water Treatment Scheme





Pretreatment Options

RO Membranes

Acid/scale inhibitor
Media filtration
Clarification/filtration
Cartridge filter



Membrane Pretreatment

- Every raw water is different
- Combination of factors can cause failures
 - Must be reliable and consistent
 - Need to solve problem early
 - Multi-Barrier Approach
 - Insurance Policy



Membrane Pretreatment Provides

- Consistent water quality to the membranes
 - Removal of potential foulants
 - Solids that are easily processed

Would Like to have:

Minimize footprint – high m/hr loading rate



Clari-DAFTM System

- Produces Consistent Water Quality Effluent
- Produces Consistently High Sludge Solids
- High loading m/hr



Impact of Clari-DAF System Pretreatment

Effluent Water Quality

- Higher Flux Rate
- Reduced Cleaning
- Higher Recovery Rate
- Protect Membrane
- Uses NO POLYMER

Solids Handling

- Less volume of sludge
- Less time to dewater
- Lower chemical cost
- Higher cake solids
- Lower disposal cost



Membrane Pretreatment Flotation Applications

- -Algae laden waters -
- -Red tide





- Organics
- Colloidal and Suspended Solids
- -Soluble Metals Fe, Mn, Al
- -Free Oil & Grease
- Cold water



Stoke's Law

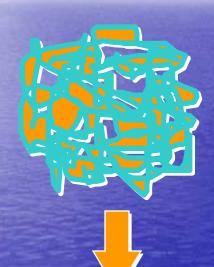
$$V = \frac{G (P1 - P2) D^2}{18 u}$$

- V = Velocity -Time to Settle/Float
 - •G = Gravity
- P1 = Particle Density

- P2 = Liquid Density
- D = Diameter of the Particle
 - u = Viscosity of the Liquid



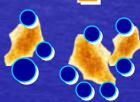
Coagulant/Polymer Addition SIZE: Tens of Microns



Buoyancy Flotation



Particle Size Difference



Gravity Settling

Bubble Addition

SIZE: Hundreds of Microns



•To develop solid process knowledge with regard to red tide / Harmful Algae Bloom removal, Leopold contracted an expert in red tide algae to grow Cochlodinium Polykrikoids, a prevalent red tide species, to

concentrations of 0.5M, 1M, and 5M cells/L.

•The Clari-DAF® process achieved excellent removal rates(>90%) at all feed concentrations.

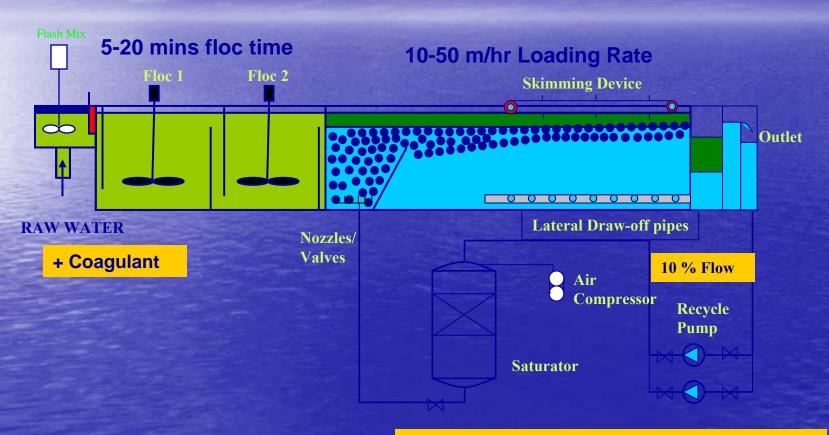
•Leopold developed a matrix of chemical dosing regimes that form the basis of sound process guarantees for our customers along with anticipated chemical consumption rates.

•Based on these experiments, Leopold optimized the Clari-DAF mechanical design to minimize capital costs while maximizing algae removal efficiencies.

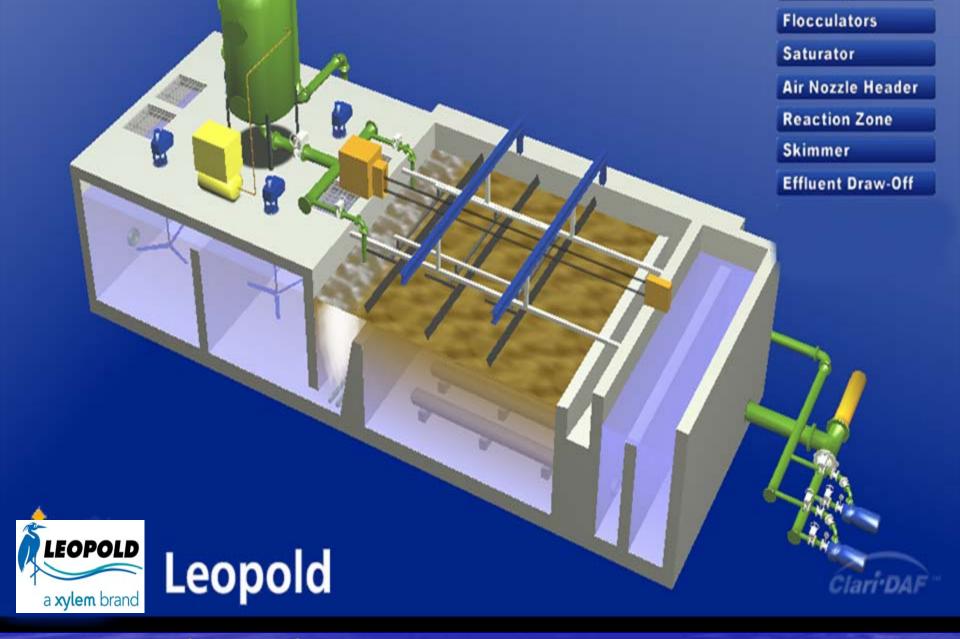




How does it Work?



Compressed Air dissolved in water at 5.5 bar



Rapid Mix

From Rapid Mix

The Clari-DAF system process starts with dosing and rapidly mixing the raw water with an aluminum or iron-based inorganic coagulant, much like conventional sedimentation. However, lower doses than sedimentation are used because a pin floc is desired instead of a sweep floc.



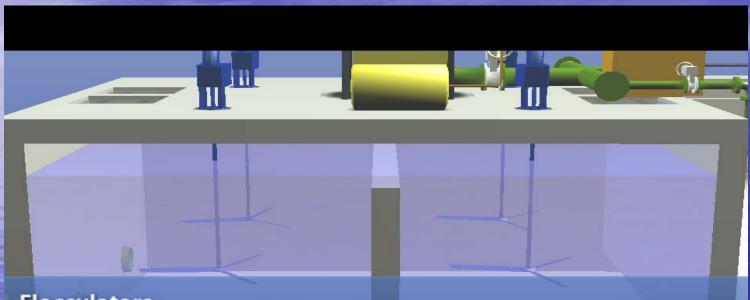
Chemical



Leopold



Flocculators

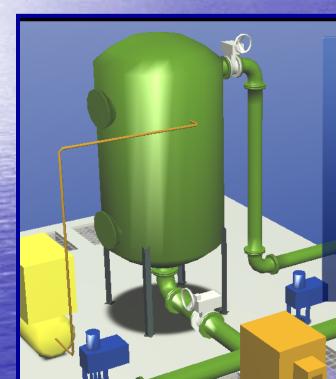


Flocculators

Good coagulation is one of the most important factors affecting flotation. Two-stage tapered flocculation is standard. G values of 30 to 100 sec⁻¹ are typical for full-scale operations. Low tip speeds prevent the fragile floc from being sheared. Flocculation time is 5 to 20 minutes depending on the source water quality.



Saturator



Saturator

The saturation process is accomplished by taking a fraction of the throughput, typically 10% of design flow, and recycling it back to a pressure vessel. VFDs control the recycle pumps so as to maintain a balance in the saturator. A compressor provides 80-psi oil-free air at a constant pressure to the saturator. The saturator, a packed tower for water or unpacked tower for wastewater system applications, collects the aerated water.





Dispersion Header Pipe





Nozzles

Air Nozzle Header

The aerated water is delivered to a distribution header that spans the width of the DAF cell. This distribution header has a series of specially designed orifices or nozzles. As the pressurized water exits the nozzles, the pressure drop produces a cloud of microbubbles that are 20 to 100 microns in size.







Reaction Zone



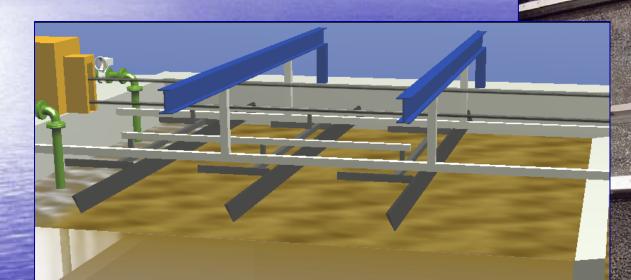
MWE PRESENTATION April, 2013

Reaction Zone

After a pin floc is formed, the raw water stream is injected with water that has been saturated with air. The contact zone is given a milky appearance like that of a whitewater blanket. The tiny air bubbles rise through the coagulated water, capturing floc as they ascend to the surface. The tiny, spherical bubbles rise under laminar flow at a rate following a modified Stokes Equation



Sludge Skimmer



Skimmer

A blanket of sludge forms on the surface of the Clari-DAF cell. The blanket is supported from beneath by the tiny air bubbles and a mechanical scraper removes the sludge blanket periodically.



Mechanical Desludging Reciprocating Skimmer

Low Maintenance 0.25 hp Motor Gentle on sludge



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<u>3% - 5% sludge solids</u>



Hydraulic De-sludging



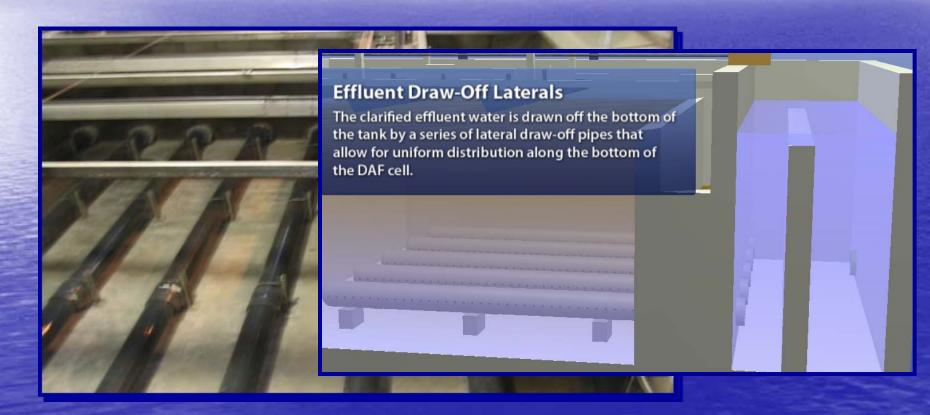
MWE PRESENTATION
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Procedure

- Effluent gate closed
- Water level rises
- Spray water starts
- Sludge flows to collection trough
- .5 1% sludge solids



Laterals





Plant	City	State	# Trains	Capacity
Fern Hill	West Chester	PA	2	3 MGD
Table Rock	Greenville	SC	12	75 MGD
Fresh Pond	Cambridge	MA	6	24 MGD
Mulgrave	Mulgrave	NS	1	0.5 MGD
Spring Canyon	Fort Collins	CO	1	0.5 MGD
Evitts Creek	Bedford	PA	3	15 MGD
Hornbine	Swansea	MA	2	0.5 MGD

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Systems Operating



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<u>Plant</u>	City	State	# Trains	Capacity
Florence	Florence	CO	2	6 MGD
Mostiste	Sobeslav	Czech Rep	2	4.6 MGD
Winnipeg	Winnipeg	Manitoba	8	105 MGD
Waco	Waco	TX	8	135 MGD
San Luis Obispo	San Luis Obispo	CA	1	7 MGD
Del Valle	Livermore	CA	1	7 MGD
Middletown	Middletown	NY	3	6 MGD



Leopold Clari-DAF SystemTM Shuwaikh SWRO, Kuwait



Commissioned in April of 2011 In Commercial Operation since October 2011



Design Parameters

- Plant Design Flow 105 MGD (16,900 m3/hr)
- 8 DAF Basins
- Basin Loading Rate 9gpm/sf (22m/hr) (collector area rate)
- Total Flocculation time of 13 Minutes
- 10% Recycle Flow



Plant Intake/Screening Structure in Foreground, Clari-DAF Building in Background



Process Notes

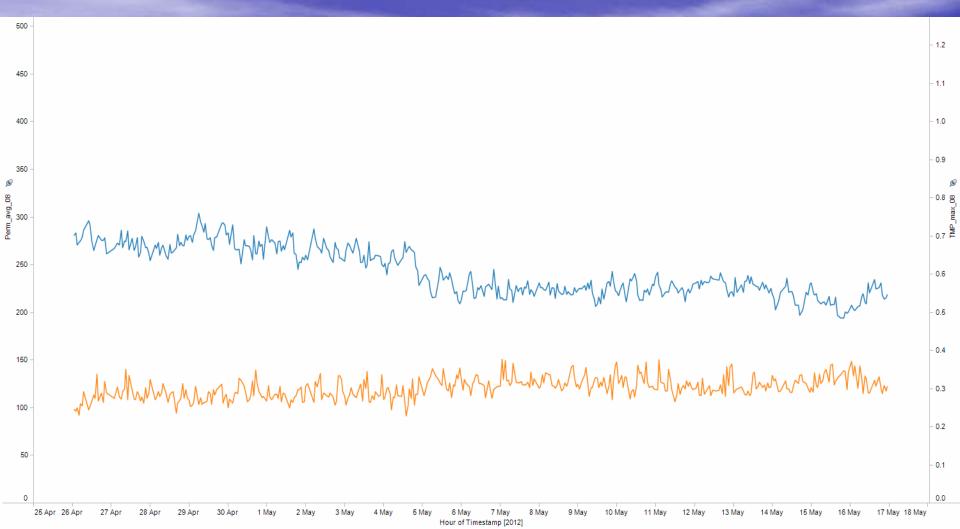
- Moderate influent turbidities averaging ~ 5 NTU since startup excursions as high 40 NTU experienced
- Red-Tide event Occurred in May 2012.
- Clari-DAF System is currently being utilized for preconditioning of UF membrane influent.
- -Typical Chemical Dose to Clari-DAF System: 2-ppm of Ferric Chloride

30-ppm of Sulfuric Acid for RO Scale Prevention

- Excellent UF Permeability and Recovery to Date



UF PERFORMANCE



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Measure Names
Perm_avg_08
TMP_max_08

- Xylem, Leopold recently completed extensive pilot testing in Oman using our state-of-the-art desalination pretreatment pilot units, which include:
 - Clari-DAF® system
 - •FilterWorx™ system single stage or 2-stage gravity media filtration.



•The source water was pulled from an existing open intake structure and was pre-chlorinated before the pilot units.

Influent turbidities ranging from 1-3 NTU and TSS <20mg/L.



Desalination Pretreatment Pilot Interior Photos



Clari-DAF® Container

FilterWorx® Container







Flocculation Clari-DAF Tank

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Filter Columns





Desalination Pretreatment – Algae Removal

•To develop solid process knowledge with regard to red tide / Harmful Algae Bloom removal, Leopold contracted an expert in red tide algae to grow Cochlodinium Polykrikoids, a prevalent red tide species, to concentrations of 0.5M, 1M, and 5M cells/L.

•The Clari-DAF® process achieved excellent removal rates(>90%) at all feed concentrations.

•Leopold developed a matrix of chemical dosing regimes that form the basis of sound process guarantees for our customers along with anticipated chemical consumption rates.

•Based on these experiments, Leopold optimized the Clari-DAF mechanical design to minimize capital costs while maximizing algae removal efficiencies.





Oman Pilot Study

with Leopold® Desalination Pretreatment Systems (Apr. to Oct. 2010)





Oman Pilot Study April-October 2010



Parameter	Averag	Min	Max
Oman R	e aw Water	Quality	
Turbidity (NTU)	1.40	0.28	6.93
рН	8.11	7.69	8.37
Temperature (°C)	31.4	28.4	33.8
Salinity (‰)	36.85	35.46	39.8 3
TSS (mg/L)	UDL	UDL	15

Scenarios Tested and Results

Parameter	Avg. SDI	
1 Stage DMF (Direct Filtration)	<4	
DAF + 1 Stage DMF	<3.5	
DAF + 2 Stage DMF	<2.5	



Algae Removal Study

with Leopold® Desalination Pretreatment Systems



Pretreatment Technologies Jar Testing for Algae Removal

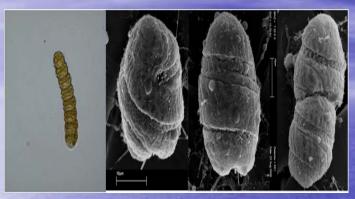
 The catastrophic 2008–2009 red tide in the Arabian gulf region, with observations on the identification and phylogeny of the fish-killing dinoflagellate Cochlodinium polykrikoides

Mindy L. Richlen a,*, Steve L. Morton b, Ebrahim A. Jamali c, Anbiah Rajan d, Donald M. Anderson a

- ^a Woods Hole Oceanographic Institution, Woods Hole, MA 02543, USA
- b NOAA/NOS Marine Biotoxin Program, 331 Ft. Johnson, Charleston, SC 29415, USA
- ^o Marine Resources Research Centre, Ministry of Environment and Water, P.O. Box-21, Umm Al Quwain, United Arab Emirates
- 4 Blodiversity Management Marine Sector, Environment Agency Abu Dhabi, P.O. Box-45553, Abu Dhabi, United Arab Emirates
- A pattern of subsequent recurrence of C. polykrikoides blooms following an initial outbreak has been observed in other parts of the world, suggesting that this species may become a persistent HAB problem in this region. As Arabian Gulf countries rely on desalination plants as the primary source of freshwater, the disruption of plant operations by recurring Cochlodinium blooms poses a serious threat to the drinking water supply in the region, and represents an unprecedented HAB impact."
- Source:

<u>http://uaeagricent.moew.gov.ae/redtide/Richlen et al Cochlodinium in the Arabian Gulf</u> 09%5B1%5D.pdf

Four Species of Algae Which Leopold has Extensively Studied in Combination with the Clari-DAF System

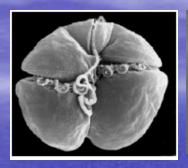


• Cochlodinium polykrikoides (20-30 பா x 30-40 பா) (**Globally)**



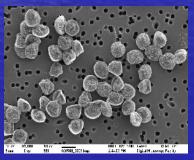


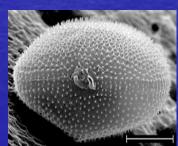
- Phaeocystis globosa (4-6 μm)
 - (Polar Oceans)





- Karenia brevis (18-45 μm)
- (Gulf of Mexico)



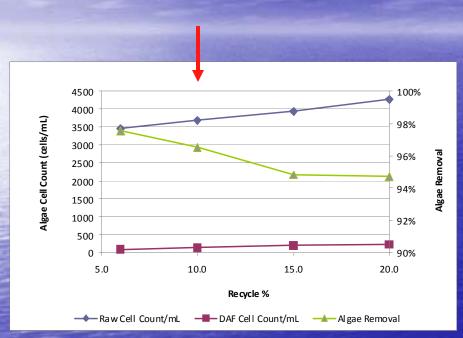


- Prorocentrum minimum
 (18-20 μ m)
 - (Europe)





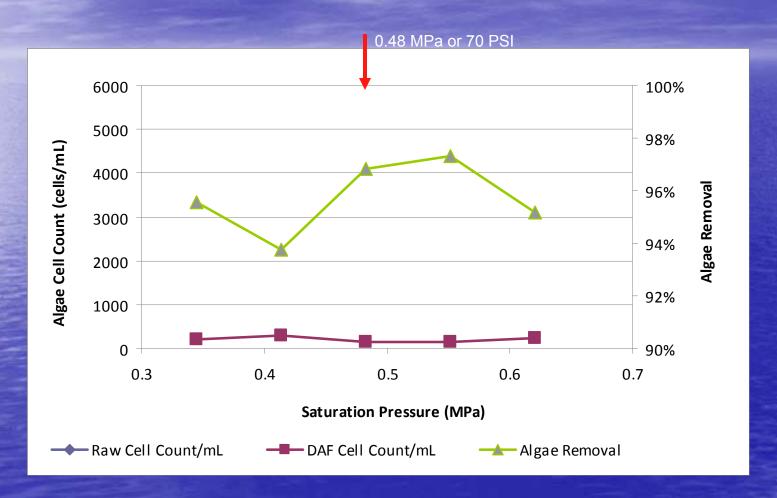
Effect of Recycle Rate







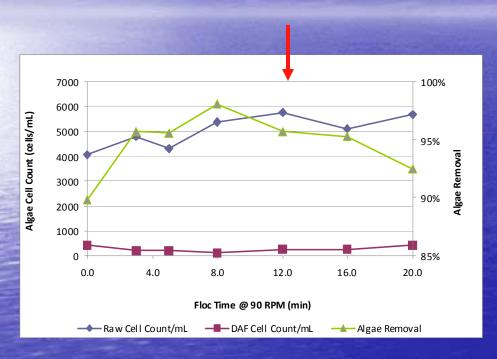
Effect of Saturation Pressure

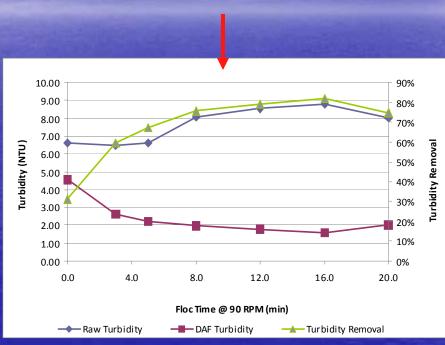




Effect of Flocculation Time

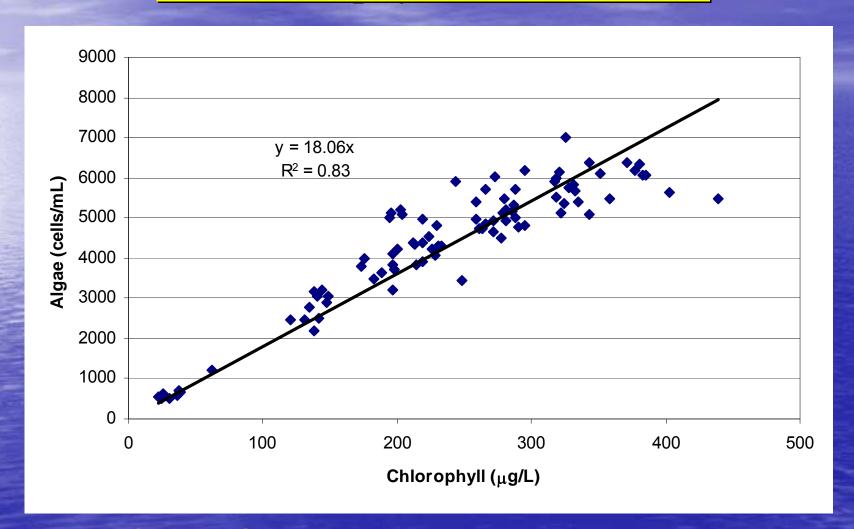






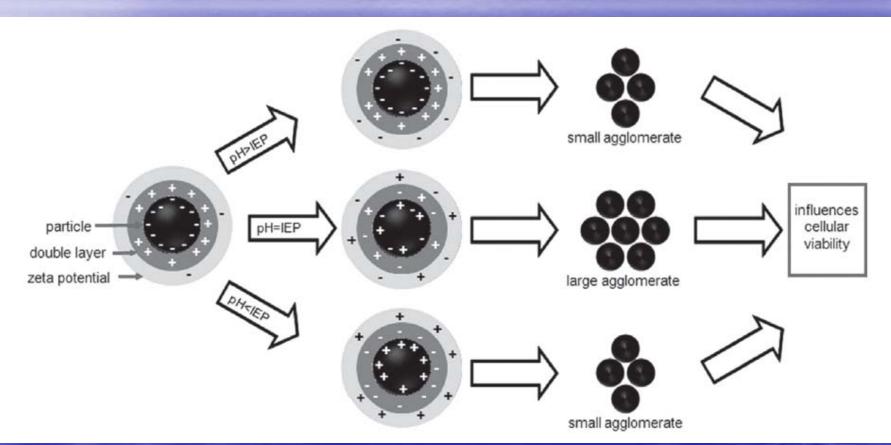


Correlation Between Algae Counts and Chlorophyll Concentrations





Conceptual Model for Effect of pH on Coagulation Applying Iso-electric Point



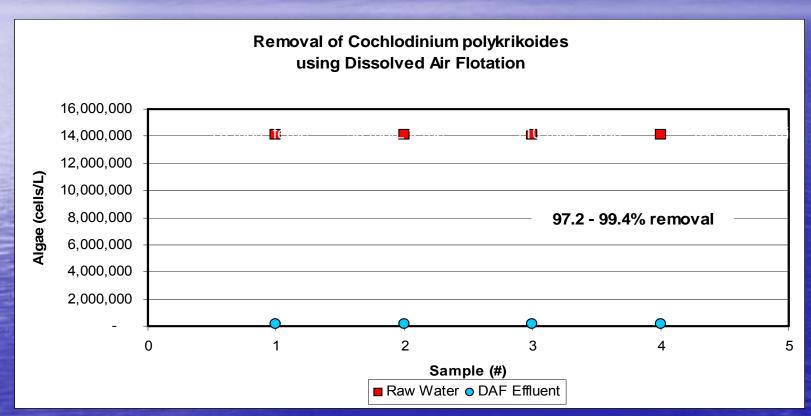


Harmful Algae Blooms (HAB) in US





Jar Test on a HAB in Buzzards Bay, MA in the USA (Aug, 2011)





Study on a HAB at Port Aransas TX Species: Karenia brevis (Nov., 2011)

0.1-0.4 Million cells/L Diameter 18-45 µm









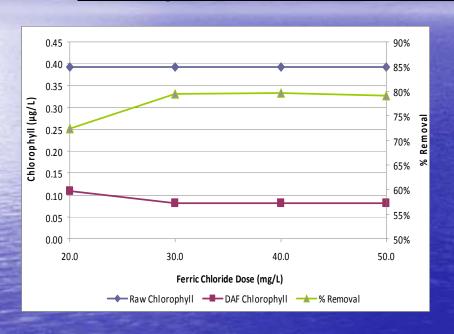


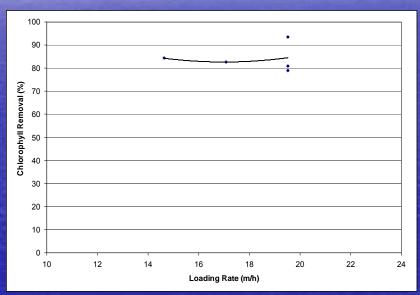






Study at Port Aransas TX (Nov., 2011)





Bench Scale Test (Gt 80160)

Pilot Scale Test (Gt 80160) (loading based on total flotation basin)



Pretreatment Technologies Oil Removal

- To further Leopold's process knowledge base, oil removal studies have also been performed.
 - ≥99% removal of free oil was obtained at concentrations of 100 mg/L
 - Further testing has shown >95% removal is also achievable with emulsified oil.

Testing indicated that mechanical design parameter for optimum algae removal are also ideal oil removal.



Study on a HAB at Port Aransas TX (Nov., 2011)

Species: Karenia brevis









- Bench scale DAF and pilot scale DAF achieved comparable removal efficiency indicating process scaling up was feasible
- With pH adjustment the coagulant dosage was reduced by half while achieving the same removal efficiency.
- Even though the depth of the flotation cell was only 5 feet deep (1.5 m), a hydraulic loading rate as high as 24 m/h (based on Collector Area) was proved feasible for algae removal.