Lecture 3: Water Softening

Water Treatment Technology

Water Resources Engineering Civil Engineering ENGC 6305

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1. Hardness definition:

- A. Hardness is the term often used to characterize a water that:
 - ü Dose form a foam or lather well and cause soap scum

$$Ca^{2+} + (Soap)^{-} \leftrightarrow Ca(Soap)_{2 (s)}$$

This increase the amount of soap needed for washing

- ü cause scaling on pipes and hot boilers.
- ü cause valves to stick due to the formation of calcium carbonate crystals
- ü leave stains on plumbing fixtures

B. Hardness is defined as the sum of the divalent metal cations (in consistent units) existing in water such as:

Ca ²⁺ , Mg ²⁺ , Fe ²⁺ , Mn ²⁺

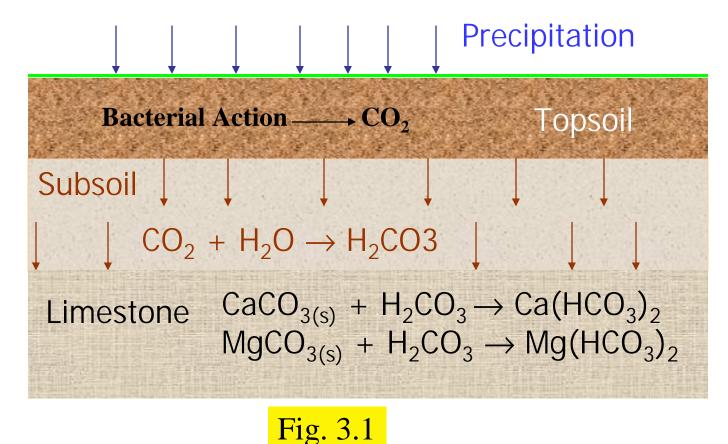
Practically most hardness is due to Ca ²⁺, Mg ²⁺ ions (the predominant minerals in natural waters)

C. Total Hardness = Ca^{2+} hardness+ Mg^{2+} hardness where the concentration of each ion is in consistent units such as mg/L as Ca^{2+} or meq/L.

D. Hard water classification

Description	Hardness range		
	(mg/L as CaCO ₃)		
Soft	0 - 75		
Moderately hard	75 - 100		
Hard	100 - 300		
Very hard	> 300		

E. Formation of Hardness



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F. Carbonate and non carbonate Hardness

- Carbonate Hardness (CH)
 - Ca²⁺, Mg²⁺ associated with HCO₃-, CO₃²⁻
 - Often called "temporary hardness" because heating the water will remove it. When the water is heated, the insoluble carbonates will precipitate and tend to form bottom deposits in water heaters.
- Non-Carbonate Hardness (NCH)
 - Ca^{2+} , Mg^{2+} associated with other ions, Cl^- , NO_3^- , SO_4^{2-}
 - NCH = TH CH

F. Hardness Units

Total Hardness = $\sum (Ca^{2+} + Mg^{2+})$

The hardness unit is the same as that consistent unit used for both of the above ions. The most used units are:

a.
$$\text{mg/L}$$
 as CaCO $_3 = (\text{mg/L}$ as species $)\frac{\text{EW of CaCO}_3}{\text{EW of species}}$

EW = equivalent weight

Species = Ion or Radical or Compound

Radical: such as CO₃²⁻, SO₄²⁻

Compounds: such as CO₂, CaSO₄

$$EW = \frac{MW}{Electrical Charge}$$

$$EW = \frac{MW}{Valance}$$

For ions

MW = molecular weight of the Species

Example 3.1: a) Find the EW of Mg ²⁺ that has a concentration of 10 mg/L as the ion in water. b) Find the EW of CaCO₃ c) find concentration of Mg ²⁺ as mg/L CaCO₃.

a) Finding the EW for Mg ²⁺:

$$MW = 24.3 \frac{g}{\text{mole}} \longrightarrow MW = 24.3 \frac{\text{mg}}{\text{mmole}}$$

$$Valance (n) = \frac{2 \text{ eq}}{\text{mole}} \longrightarrow Valance (n) = \frac{2 \text{ meq}}{\text{mmole}}$$

$$EW = \frac{MW}{Valance} \longrightarrow EW = \frac{24.3 \text{ mg}}{\text{mmole}} \cdot \left[\frac{1}{2 \text{ meq/mmole}}\right] \longrightarrow EW = 12.15 \frac{\text{mg}}{\text{meq}}$$

b) Finding the EW for CaCO₃:

$$MW = 100 \quad \frac{g}{\text{mole}} \quad \longrightarrow \quad MW = 100 \quad \frac{\text{mg}}{\text{mmole}}$$

Electrical charge (n) =
$$\frac{2 \text{ eq}}{\text{mole}}$$
 Electrical charge = $\frac{2 \text{ meq}}{\text{mmole}}$

$$EW = \frac{MW}{Electrical Charge} \longrightarrow EW = \frac{100 \text{ mg}}{mmole} \cdot \left[\frac{1}{2 \text{ meq/mmole}}\right] \longrightarrow EW = 50 \frac{mg}{meq}$$

D) Finding the Mg $^{2+}$ concentration as CaCO₃:

mg/L as CaCO₃ = (mg/L as species)
$$\frac{\text{EW of CaCO}_3}{\text{EW of species}}$$
 Mg ²⁺ conc.

(Mg2+) in mg/L as CaCO₃ = (10 mg/L as Mg 2+) $\frac{50 \text{ mg/meq}}{12.15 \text{ mg/meq}}$ \longrightarrow 41.15 mg/L as CaCO₃

NAME	SYMBOL OR FORMULA	ATOMIC OR MOLECULAR WEIGHT	EQUIVALENT WEIGHT
Aluminum	Al ³⁺	27.0	9.0
Calcium	Ca ²⁺	40.1	20.0
Carbon	C	12.0	
Hydrogen	\mathbf{H}^{+}	1.0	1.0
Magnesium	Mg ²⁺	24.3	12.2
Manganese	Mn^{2+}	54.9	27.5
Nitrogen	N	14.0	
Oxygen	O	16.0	20
Phosphorus	P	31.0	
Sodium	Na ⁺	23.0	23.0
Ammonium	NH_4^+	18.0	18.0
Bicarbonate	HCO ₃ -	61.0	61.0
Carbonate	CO_3^{2-}	60.0	30.0
Hydroxyl	OH-	17.0	17.0
Hypochlorite	OCI-	51.5	51.5
Nitrate	NO ₃ -	62.0	62.0
Orthophosphate	PO ₄ 3-	95.0	31.7
Sulfate	SO ₄ ²⁻	96.0	48.0
Aluminum hydroxide	Al(OH) ₃	78.0	26.0
Calcium bicarbonate	Ca(HCO ₃) ₂	162	81.0
Calcium carbonate	CaCO ₃	100	50.0
Calcium sulfate	CaSO ₄	136	68.0
Carbon dioxide	CO_2	44.0	22.0
Ferric hydroxide	Fe(OH) ₃	107	35.6
Hydrochloric acid	HCl	36.5	36.5
Magnesium carbonate	MgCO ₃	84.3	42.1
Magnesium hydroxide	$Mg(OH)_2$	58.3	29.1
Magnesium sulfate	$MgSO_4$	120	60.1
Sodium sulfate	Na ₂ SO ₄	142	71.0

b.
$$eq/L = \frac{g/L \text{ as ion}}{EW \text{ of the ion}}$$

or
$$meq/L = \frac{mg/L \text{ as ion}}{EW \text{ of the ion}}$$

$$eq/L = \frac{g/L \text{ as Compound or Radical}}{EW \text{ of the Compound or Radical}}$$

or

$$meq/L = \frac{mg/L \text{ as Compound or Radical}}{EW \text{ of the Compound or Radical}}$$

Example 3.3: for example 3.1 find the concentration of Mg $^{2+}$ as meq/L.

$$meq/L = \frac{mg/L \text{ as ion}}{EW \text{ of the ion}}$$

$$(Mg2+) \text{ concentration} = \frac{10 \text{ mg/L as (Mg2+)}}{12.15 \text{ mg/meq}}$$

$$= 0.82 \text{ meq/L}$$

$$Mg^{2+} \text{ conc.}$$

F. Alkalinity

Alkalinity is a very important parameter in water chemistry and related very closely to hardness and softening process. The following equation is used to measure the alkalinity in water:

- Alkalinity = $(HCO_3^-) + (CO_3^{2-}) + (OH^-) (H^+)$
 - Where the concentrations are in meq/L or mg/L as CaCO₃ Usually the (OH-) and (H+) are negligible.
- The relation between the alkalinity species is given by the following three equations:

$$10^{-10.33} = \frac{[H^+][CO^{2-}_{3}]}{[HCO3-]}, \quad 10^{-14} = [H^+] \bullet [OH^-], \quad [H^+] = 10^{-pH}$$

Where the concentrations are moles/ L in these three equations

Various Forms of alkalinity and CO₂ relative to pH in water at 25 °C.

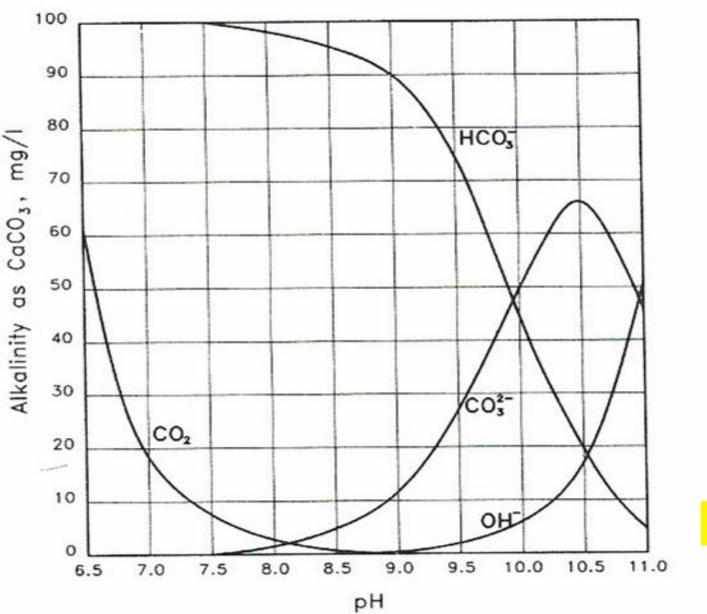


Fig. 3.2

Example 3.3

• A sample of water having a pH of 7.2 has the following concentrations of ions

- Construct a bar chart of the ions in term of mg/L CaCO₃
- Calculate the TH, CH, NCH, Alkalinity

Example 3.3 ..cont'

Ion	Conc.	M.W.	n	Eq. Wt.	Conc.	Conc.
	mg/L	mg/mmol		mg/meq	meq/L	mg/L as
						CaCO ₃
Ca ²⁺	40.0	40.1	2	20.05	1.995	99.8
Mg ²⁺	10.0	24.3	2	12.15	.823	41.2
Na ⁺	11.8	23.0	1	23.0	.51	25.7
K ⁺	7.0	39.1	1	39.1	.179	8.95
HCO ₃	110.0	61.0	1	61.0	1.80	90.2
SO_4^{2-}	67.2	96.1	2	48.05	1.40	69.9
Cl	11.0	35.5	1	35.5	.031	15.5

Note: Examples 3.1 and 3.2 are sample calculations for Mg ²⁺ in this Example

Example 3.3 ..cont'

Check The ionic balance:

```
\Sigma(cations) = \Sigma(anions)

175.6 = 175.6 \quad \text{mg/L as CaCO}_3 \quad \text{O.K}

3.51 = 3.23 \quad \text{meq/L} \quad \text{O.K}
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Note: (error in the range of \pm 10% is accepted)

Note: one check is enough (either as {mg/L as CaCO3} or as {meq/L})

• Total Hardness =
$$\Sigma$$
 (Ca²⁺) + (Mg²⁺)= 99.8 + 41.2
TH =141 mg/L as CaCO₃
or — TH= 1.995 + 0.823 = 2.818 meq/L

Example 3.3 ..cont'

- Alkalinity = $(HCO_3^-) + (CO_3^{2-}) + (OH^-) (H^+)$
- **a.** Since pH = 7.2 \rightarrow [H⁺] = 10^{-pH} = 10^{-7.2} mole/L = 10^{-7.2} g/L

$$eq/L = \frac{g/L \text{ as ion}}{EW \text{ of the ion}} = \left[eq/L = \frac{10^{-7.2} \text{ g H}^+/L}{1 \text{ g/eq}} \right] \longrightarrow \left[(H^+) = 10^{-7.2} \text{ eq/L} \right]$$

b.
$$10^{-14} = [H^+] \bullet [OH^-]$$
 $= 10^{-14} = 10^{-7.2} \bullet [OH^-]$ $\longrightarrow [OH^-] = 10^{-6.8} \text{ mole/L}$

$$[OH^{-}] = 10^{-6.8} \text{ mole/L} = 17*10^{-6.8} \text{ g/L} \longrightarrow eq/L = \frac{17*10^{-6.8} \text{ g OH}^{-}/L}{17 \text{ g/eq}} \longrightarrow (OH^{-}) = 10^{-6.8} \text{ eq/L}$$

<u>c.</u> (HCO₃-) = 1.80 meq/L = $\underline{1.80 * 10^{-3} \text{ eq/L}}$ from this example calculations as in the table.

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g/L as HCO<sub>3</sub><sup>-</sup> = EW * eq/L = (61 g/eq) * 1.80 *10<sup>-3</sup> g/L = 109.8 * 10<sup>-3</sup> g/L [HCO<sub>3</sub><sup>-</sup>] = (109.8 * 10<sup>-3</sup> g/L)/(61 g/mole) = 1.80 *10<sup>-3</sup> mole/L
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Example 3.3 ..cont'

d. Find the carbonate concentration:

$$10^{-10.33} = \frac{[H^+][CO_3^{2-}]}{[HCO3-]} \longrightarrow 10^{-10.33} = \frac{10^{-7.2} \times [CO_3^{2-}]}{1.8 \times 10^{-3}}$$

[CO₃²⁻]= 1.33 x 10⁻⁶ mole/L = 79.8 x 10⁻⁶ g/L
CO₃²⁻ in eq/L =
$$\frac{79.8*10^{-6} \text{ g/L}}{30 \text{ g/eq}}$$
 = 2.66 x 10⁻⁶ eq/L

Alkalinity =
$$(1.80 \times 10^{-3}) + (2.66 \times 10^{-6}) + 10^{-6.8} - 10^{-7.2} = 1.801 \times 10^{-3} \text{ eq/L}$$

Alkalinity =
$$1.801 \text{ x } 10^{-3} \text{ x } 1000 \text{ x } 50 = 90.1 \text{ mg/L as } \text{CaCO}_3$$

Note: it is clear that the most effective form of alkalinity is bicarbonate, this is always true when the pH is 8.3 or less.

Example 3.3 ..cont'

Carbonate Hardness

the portion of the hardness associated with carbonate or bicarbonate

- Alkalinity = 90.1 mg/L as $CaCO_3$

$$TH = 141 \text{ mg/L as } CaCO_3$$

$$CH = 90.2 \text{ mg/L as } CaCO_3$$

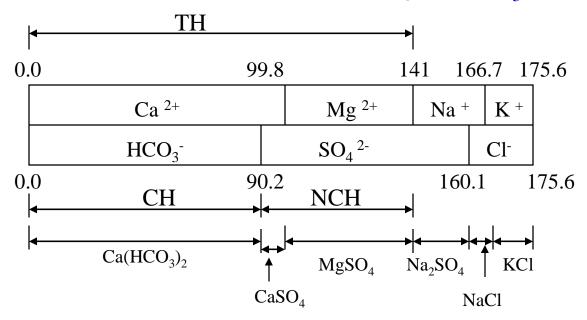
- Non-carbonate Hardness:

$$NCH = TH - CH$$

= 141 - 90.1= 50.9 mg/L as CaCO₃

Example 3.3 ..cont'

Construct the bar chart of the ions in term of mg/L CaCO₃



Note: the chemicals at the lower line of the bar graph is called the <u>hypothetical</u> combination of positive and negative ions in the water sample

2. Softening definition:

- Softening is the chemical processes in which hardness causing ions (Ca²⁺, Mg²⁺) are removed from water ether completely or partially.
- b) Softening may be a chivied by chemical precipitation using the Lime-Soda Ash method or by ion exchange.
- c) In the chemical precipitation method the objective is to produce CaCO₃ and Mg(OH)₂:

$$Ca^{2+} + CO_3^{2-} \leftrightarrow 2CaCO_{3(s)}$$

$$Mg^{2+} + 2OH^- \leftrightarrow Mg(OH)_{2(s)}$$

These two reactions are achieved by the addition of Lime [Ca(OH)₂] and Soda ash [Na₂CO₃] as will be shown.

- f) A common water treatment goal is to provide a water with a hardness in the range of 75 to 120 mg/L as CaCO₃
- g) To precipitate $CaCO_3$ and $Mg(OH)_2$ we need to raise the pH to 10.3 by the addition of Lime $[Ca(OH)_2]$. The addition of the OH- will convert HCO_3^- to CO_3^{2-}
- h) To precipitate $Mg(OH)_2$ we need to raise the pH to 11 by the addition of Soda ash [Na_2CO_3]. This will add the CO_3^{2-} ion needed to react with the remaining Ca $^{2+}$
- i) Some of the added lime $[Ca(OH)_2]$ is consumed to remove CO_2 which is necessary to raise the pH.

3. Chemistry of Lime- Soda Ash Softening

3.1) softening reactions

- Neutralization of carbonic acid
 [To raise the pH we need first to neutralize any acid in the water]
 CO₂ + Ca(OH)₂ ↔ CaCO_{3(s)} + H₂O
- Precipitation of CH due to calcium: [To raise the pH to 10.3 all the HCO_3^- is converted to CO_3^{2-}] $Ca^{2+} + 2HCO_3^- + Ca(OH)_2 \leftrightarrow 2CaCO_{3(s)} + 2H_2O$
- Precipitation of CH due to magnesium
 [To raise the pH to 11 add more lime]

$$\begin{split} Mg^{2+} + 2HCO_3^{-+} + \frac{\text{Ca(OH)}_2}{\text{Ca(OH)}_2} &\longleftrightarrow Mg^{2+} + CO_3^{2-} + \text{CaCO}_{3(s)} + 2H_2O \\ Mg^{2+} + CO_3^{2-} + \frac{\text{Ca(OH)}_2}{\text{Ca(OH)}_2} &\longleftrightarrow MgOH_{2(s)} + \text{CaCO}_{3(s)} \end{split}$$

Removal of NCH due to calcium

$$\begin{aligned} &Ca^{2+} + SO_4^{-2} + Na_2CO_3 \Longleftrightarrow CaCO_{3(s)} + 2Na^+ + SO_4^{-2} \\ &Ca^{2+} + 2Cl^{-1} + Na_2CO_3 \Longleftrightarrow CaCO_{3(s)} + 2Na^+ + 2Cl^{-1} \end{aligned}$$

• Removal of NCH due to magnesium

$$Mg^{2+} + Ca(OH)_2 \leftrightarrow MgOH_{2(s)} + Ca^{2+}$$

 $Ca^{2+} + Na_2CO_3 \leftrightarrow CaCO_{3(s)} + 2Na^+$

3.2) Softening process limitations:

- 1. Lime-Soda softening cannot produce a water completely free of hardness because of the solubility of CaCO₃ and Mg(OH)₂, limitations of mixing and reaction time.
- 2. Thus, the minimum calcium hardness that can be achieved is 30 mg/L as CaCO₃, the minimum Magnesium hardness that can be achieved is 10 mg/L as CaCO₃, this gives a minimum hardness of 40 mg/L as CaCO₃.
- 3. However, normally the water is treated to give a hardness in the range of 75 to 120 mg/L as CaCO₃.
- 4. An Excess lime beyond the stoichiometric amount is usually added to remove Mg $^{2+}$ hardness . The minimum excess lime is usually 20 mg/L as CaCO $_3$, maximum excess lime is 62.5 mg/L as CaCO $_3$ (1.25 meq/L).
- 5. Mg ²⁺ in excess of 40 mg/L as CaCO₃ is not desired as it forms scale in water heaters. Mg ²⁺ is expensive to remove, so we only remove Mg ²⁺ in excess of 40 mg/L as CaCO₃.

3.3) Chemicals requirements:

According to the softening chemical reactions:

- -Lime is added at the ratio of 1:1 for each carbonate hardness compound except for Mg(HCO₃) the ratio is 2:1 [i.e. 2 lime for each 1 Mg(HCO₃)].
- -Lime is also added at the ratio of 1:1 for each Magnesium NCH compound such as MgSO₄
- -Soda ash is added at the ratio of 1:1 for each Magnesium or Calcium NCH compound such as MgSO₄, and CaSO₄.
- CO₂ needed is 1:1 ratio with the excess lime added, and 1:1 ratio with CaCO₃ remaining after softening, 2:1 ratio with Mg(OH)₂ remaining after softening.
- The units of the chemicals are either in meq/L or mg/L CaCO₃
- Example 3.4 illustrates the chemical requirements calculations.

4. Process variation in Lime Soda-Ahs softening:

There are three basic schemes for water softening:

- Excess lime treatment
- -Selective Calcium removal
- -Split treatment

4.1) Excess lime treatment:

- Carbonate hardness associated with Ca ²⁺ can be effectively removed to the practical limit of CaCO₃ (30 mg/L as CaCO₃) by adding the stoichiometric addition of lime.
- •Precipitation of hardness (CH or NCH) associated with Mg²⁺ as Mg(OH)₂ needs in addition to the stoichiometric addition of lime to an excess lime of 62.5 mg/L as CaCO₃), without it Mg(OH)₂ will not precipitate. In fact this excess lime raise the pH to 11.
- •Excess lime treatment reduces the total hardness to 40 mg/L as CaCO₃ (i.e., 30 mg/L CaCO₃ and 10 mg/L Mg(OH)₂ as CaCO₃)
- •The excess lime treatment is usually achieved in a two stage system as shown in the Figure 3.3

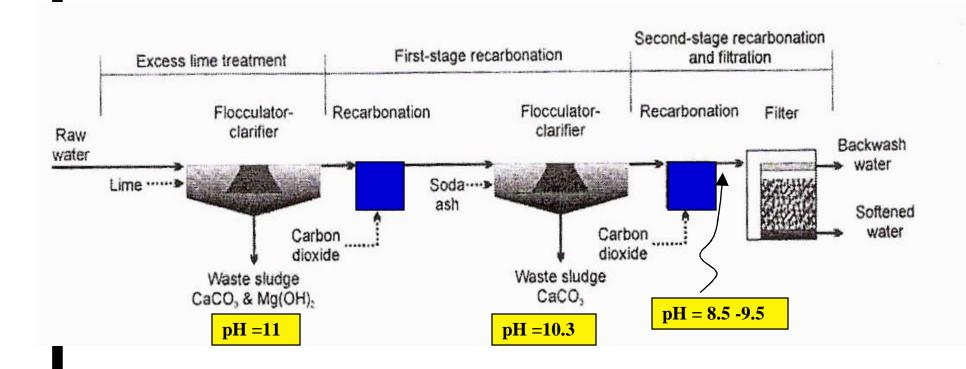


Fig. 3.3 Schematic diagram of a two stage excess lime softening water treatment plant

- The system is composed of:
 - -Rapid mixer,
 - -Flocculator/sedimentation tank,
 - -recarbonation tank,
 - Rapid mixer
 - -Second stage Flocculator/sedimentation tank
 - -second stage recarbonation tank
 - -Filtration tank
- In the first stage only lime is added to the system through a rapid mixer this will raise the pH to 11. CaCO₃ and Mg(OH)₂ will precipitate in this stage.
- Recarbonation is implemented to reduce the pH to 10.3 before interring the second stage. This reduction occurs due to the removal of the excess lime added in the first stage:

$$Ca (OH)_2 + CO_2 = CaCO_3 \downarrow + H_2O$$

Excess lime

- In the second stage only Soda Ash is added to the system through a rapid mixer. CaCO₃ will precipitate in this stage from the excess lime and from the NCH reaction.
- •Recarbonation is implemented after the second stage Flocculator /sedimentation to reduce the pH in the range of 8.5-9.5 to stabilize the water by converting some of the Ca CO₃ and Mg (OH)₂ residual to bicarbonate :

Ca
$$CO_3 + CO_2 + H_2O = Ca (HCO_3)_2$$

Mg $(OH)_2 + 2CO_2 = Mg (HCO_3)_2$

•Recarbonation is a chivied in a tank in which carbon dioxide is injected either in liquid form or in the gaseous form generated in the tank using a special burner as Shown in Figure 3.4.

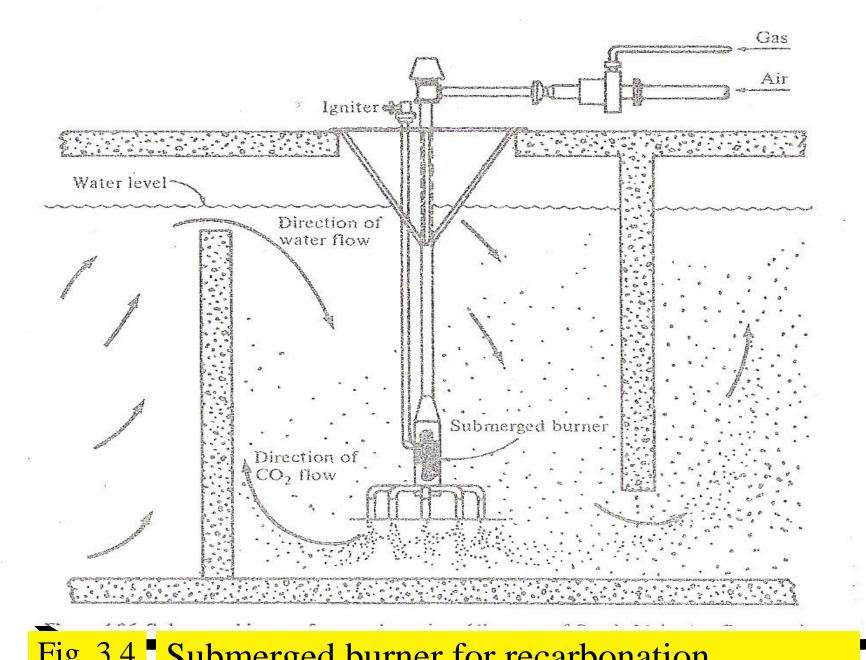
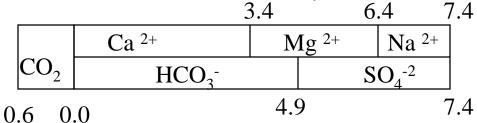


Fig. 3.4 Submerged burner for recarbonation

- •The first stage removes the following:
 - CH hardness associated with Ca²⁺
 - -CH and NCH associated with Mg²⁺
 - Recarbonation reduces pH from 11 to 10.3
- The Second stage removes the following:
- -NCH hardness associated with Ca ²⁺ that is originally existing in water
- -NCH hardness associated with Ca ²⁺ that was created from the first stage.
- -Recarbonation reduces pH from 10.3 to the range 8.5-9.5

Example: 3.4

A water with the ionic characteristics shown below is to be softened to the minimum possible hardness by the two stage lime-soda-ash excess lime process. Calculate the required chemical quantities in meq/L. Draw a bar diagram of the finished water. Assume that 0.6 meq/L CaCO₃ and 0.2 meq/L Mg(OH)₂ will be in the effluent of the second stage before recarbonation. Assume also that 0.2 meq/L Mg(OH)₂ and 0.2 meq/L of the 0.6 CaCO₃ will be converted to HCO₃-by second stage recarbonation to reach water stability.



Solution:

Lime =
$$0.6+3.4+2(4.9-3.4)+(6.4-4.9)+$$
 excess lime = $8.5+1.25=9.75$ meq/L
Soda Ash = $6.4-4.9=1.5$ meq/L (to remove NCH, MgSO₄²⁻)

Example: 3.4 Cont'

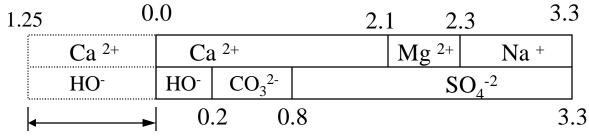
<u>CO₂:</u>

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1^{\text{st}} stage recarbonation = 1.25 meq/ L [to remove the excess lime] 2^{\text{nd}} stage recarbonation = 0.2 meq/L [to convert 0.2meq/L of CaCO<sub>3</sub> to Ca(HCO<sub>3</sub>)] + (0.20 \text{ x } 2) meq/L [to convert all Mg(OH)<sub>2</sub> to Mg(HCO<sub>3</sub>)]= 0.60 meq/L] Total CO<sub>2</sub> needed = 1.25+0.6 = 1.85 meq/L
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<u>Na + :</u>

- The addition of soda ash adds to the water an equal amount of Na⁺.
- Since we added 1.5 meq/L soda ash, this will add 1.5 meq/L Na⁺
- The original concentration existing in the raw water is 1.0 meq/L . Total $Na^+ = 1 + 1.5 = 2.5$ meq/L Na^+ .

Example: 3.4 Cont'

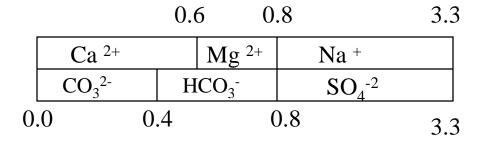


Excess lime

Bar graph of the water before recarbonation and before adding Soda -Ash

Bar graph of the water after adding Soda –Ash and 1st stage recarbonation

Example: 3.4 Cont'



Bar graph of the finished water after and 2nd stage recarbonation

The remaining hardness:

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Calcium hardness = 0.6 \text{ meq/L} = 30 \text{ mg/L} as CaCO_3
Calcium hardness = 0.2 \text{ meq/L} = 10 \text{ mg/L} as CaCO_3
TH remaining = 0.8 \text{ meq/L} = 10 \text{ mg/L} as CaCO_3
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4.2) Selective Calcium removal:

- -Magnesium hardness is expensive to remove.
- -Only Magnesium hardness in excess of 40 mg/L as CaCO₃ (0.8 meq/l) needs to be removed.
- For waters having an Mg ²⁺ hardness less or equal to 40 mg/L CaCO₃, only Ca²⁺ hardness needs to be removed.
- to remove only Ca ²⁺, we add lime needed to remove Ca 2+, and do not add excess lime. In this way no Mg²⁺ removal occurs.
- -Soda Ash may be needed if NCH associated with Ca²⁺ is to be removed.
- -That's way this treatment is called selective.
- -This treatment is achieved in a single stage system as that shown in Figure 3.5

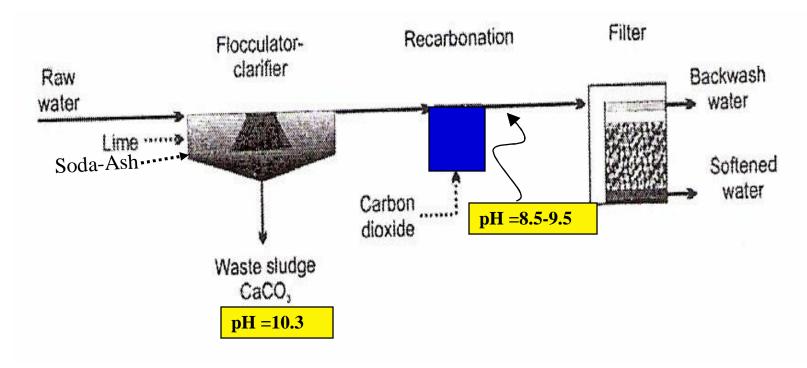


Fig. 3.5 Schematic diagram of a single stage softening water treatment plant

Example: 3.5

A water with the ionic characteristics shown below is to be softened by selective calcium process. Calculate the required chemical quantities in meq/L. Draw a bar diagram of the finished water.

0.4 0.0				3.5	4.	3 4	4.6
	CO_2	Ca ²⁺			Mg ²⁺	Na ²⁺	
		HCO ₃ -		•	SO_4^{-2}	Cl-1	
0	.4 0	.0	2.3		4	.3	4.6

Solution:

Since Mg²⁺ is 0.8 meq/L we can apply the selective calcium treatment.

Lime =
$$0.4 + 2.3 = 2.7$$
 meq/L [to remove CO₂ and Ca(HCO₃) only]
= $2.7 \times 28 = 76$ mg/L CaO
Soda Ash = $3.5 - 2.3 = 1.2$ meq/L [to remove NCH, CaSO₄]
= $1.2 \times 53 = 64$ mg/L Na₂CO₃

Example: 3.5 Cont'

<u>CO</u>₂:

For stability reasons it is desired to convert 0.3 out of the 0.6 meq/L $CaCO_3$ to $Ca(HCO_3)_2$ by recarbonation.

Recarbonation = $0.3 \text{ meq/} \text{ L CO}_2$ [to convert $0.2 \text{meq/L of CaCO}_3$ to Ca(HCO₃)] = $0.3 \times 22 = 6.6 \text{ mg/L CO}_2$

<u>Na + :</u>

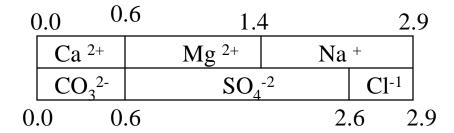
- The addition of soda ash adds to the water an equal amount of Na⁺.
- Since we added 1.2 meq/L soda ash, this will add 1.2 meq/L Na⁺
- The original concentration existing in the raw water is 0.3 meq/L.

Total
$$Na^+ = 0.3 + 1.2 = 1.5 \text{ meq/L Na}^+$$

= 1.5 x 23 = 34.5 mg/L Na^+

Final hardness = all the original Mg
$$^{2+}$$
 + 0.6 meq/L calcium hardness = 0.8 meq/L Mg $^{2+}$ + 0.6 meq/L Ca $^{2+}$ = 1.4 meq/L = 1.4 X 50 = 70 mg/L CaCO₃

Example: 3.5 Cont'



Bar graph of the water after softening and before recarbonation

Bar graph of the finished water after recarbonation

4.3) Split Treatment:

- Split treatment consist of treating portion of the raw water by excess lime treatment and Then neutralizing the excess lime by the bicarbonate naturally existing in the untreated bypass flow (Figure 3.6).
- The first stage is operated to soften the water to the practical limits of 10 mg Mg^{+2}/L as $CaCO_3$, and 30 mg Ca^{2+}/L as $CaCO_3$
- Magnesium concentration in the bypass will be the same as in the raw water.
- The finished water should have a final of 40 mg Mg⁺²/L as CaCO₃ as desired by domestic water users and industries.
- <u>Some advantages of Split Treatment:</u>
 - * Reduces the chemical dosage of lime and CO₂.
 - * No need for first stage recarbonation
 - * Reduce the capital cost of the first stage since only a portion of the water is treated and consequently the tanks are smaller.
 - * Allows us to leave a Mg ²⁺ concentrations above the practical value of 10 10 mg Mg⁺²/L as CaCO₃ usually we are forced to achieve in the conventional excess lime treatment.

-The Fraction Bypassed is calculated as:

$$X = \frac{Mg_f - Mg_i}{Mg_r - Mg_i}$$

Where, Mg_f = final magnesium concentration, mg/L $CaCO_3$

 Mg_i = magnesium concentration from the first stage, mg/L CaCO₃

 Mg_r = raw water magnesium concentration, mg/L CaCO₃

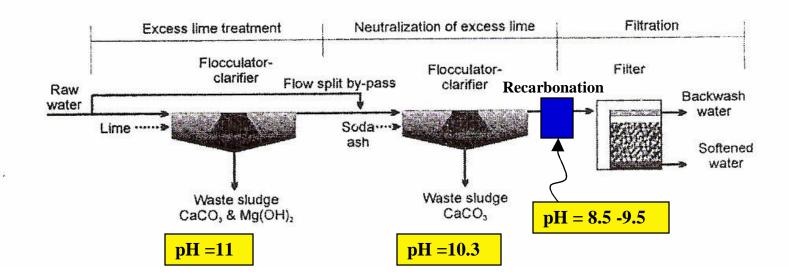


Fig. 3.6 Schematic diagram of a split system softening water treatment plant

Example: 3.6

For the water in example 3.4 use a split treatment to soften it. Calculate the required chemical quantities in meq/L. Draw a bar diagram of the finished water. Assume that the maximum permissible Magnesium hardness of 40 mg/L $CaCO_3$ and Calcium hardness in the range of 40-60 mg/L $CaCO_3$. The expected magnesium hardness from the first stage split is $10 \text{ mg/L } CaCO_3$.

Solution:

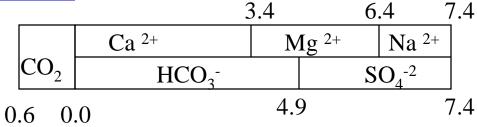
$$X = \frac{Mg_f - Mg_i}{Mg_r - Mg_i}$$
 \longrightarrow $X = \frac{40 - 10}{3(50) - 10} = 0.214$

$$1 - X = 1 - 0.214 = 0.786$$

Example: 3.6 Cont' Solution: Chemicals to be added A) Lime = 0.786 [(0.6 + 3.4 + 2(4.9 - 3.4) + (6.4 - 4.9)]= 6.681 meq/L [needed for the first stage treatment] Lime = 0.214 [0.6 + 3.4] = 0.856 meq/L [needed for removing the Ca ²⁺ hardness and CO₂ from the bypass flow. However, this amount will be added to the first stage, and will act as an excess lime.] Excess lime concentration in the first stage = (0.856/0.786) = 1.09 < 1.25 meq/Lso additional amount is needed $= Y/0.786 = 1.25 \longrightarrow Y = 0.983 \text{ meg/L}$ $= 0.214 [0.6 + 3.4 + Z] = 0.983 \longrightarrow Z = 0.593 \text{ meg/L}$ Corrected lime for the bypass = 0.214[0.6+3.4+0.593]=0.983 meq/LExcess lime concentration in the first stage = (0.983/0.786) = 1.25 meq/L (OK). B) Soda Ash = See the lower Bar graph in slide 48, we need to remove $CaSO_4$ = 1.3-0.60 = 0.70 meq/LAnother method to calculate the needed Soda Ah: Soda ash =(Raw water Mg ²⁺ concentration - 0.80) meq/L Mg ²⁺ NCH + meq/L Ca ²⁺ NCH = 1.50 - 0.80 + 0.0

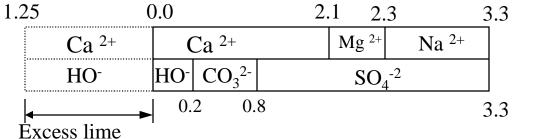
= 0.70 meq/L

Example: 3.6 Cont'





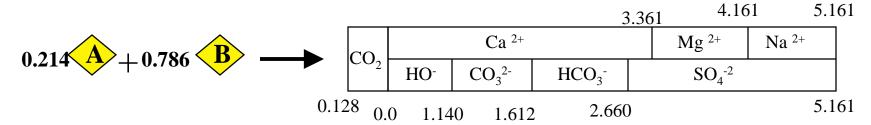
Bar graph of the water in the Bypass line (Raw water)





Bar graph of the water after the first stage split softening before blending and before adding Soda Ash

Example: 3.6 Cont'



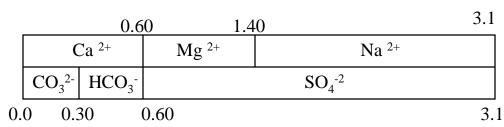
Bar graph of the water after blending and before reaction between the excess lime and before adding Soda Ash

Bar graph of the water after blending and reaction between the excess lime and before adding Soda Ash

Example: 3.6 Cont'

_	0.6	50 1.4	.0	3.1
	Ca ²⁺	Mg ²⁺	Na ²⁺	
	CO ₃ ²⁻		SO ₄ -2	
0.0	0.6	0		3.

Bar graph of the water after adding Soda Ash and before second stage carbonation



Bar graph of the finished water

Note:

Remaining hardness = $0.60 \text{ Ca}^{2+} \text{ hardness} + 0.8 \text{ Mg}^{2+} \text{ hardness} = 1.40 \text{ meq/L}$

= 0.60X 50 mg Ca ²⁺ /L CaCO₃ + 0.8 Mg ²⁺ mg/L CaCO₃

= $30 \text{ mg Ca}^{2+}/\text{L CaCO}_3 + 40 \text{ mg Mg}^{2+}/\text{L CaCO}_3$

Remaining Hardness = $70 \text{ mg} / \text{L CaCO}_3$

5. Coagulation and Softening

- The softening precipitates [i.e. CaCO₃ and Mg(OH)₂] may be more efficiently removed by adding a coagulant such as Alum.
- On the other hand, if both coagulation and softening are to be applied ,(such as in hard turbid surface water), the coagulation process is more efficient due to the greater quantity of precipitate formed due to softening.
- That's why coagulation and lime soda-Ash softening have similar infrastructure (i.e. rapid mixer, Flocculator, sedimentation tank).