<u>Using API-617 as a Purchase Specification</u> <u>for Centrifugal Compressors</u>

Although they are not legal documents, the various standards compiled and issued by the American Petroleum Institute (API) reflect the experience and recommendations of both users' and manufacturers' groups. These groups wish to impart safety and reliability to equipment utilized in the hydrocarbon processing industry (HPI). Of the two most important standards used in procuring dynamic compression machinery, API-617 pertains to centrifugal compressors and API614 applies to lubricating-oil systems. Virtually all API standards require users to make decisions on clauses marked with bullets (•), and understanding the standards is important for all parties. Therefore, highlighting a few clauses with explanatory remarks will be helpful in using the 7th Ed. (2002) API-617. (It should be noted that the numeric designation of a certain clause may change as the API Standard undergoes progressive updating or revisions.)

| Clauses(s) | Торіс | API Explanation | Remarks |
|----------------|--|---------------------------------|-------------------------------------|
| 1.5.18 through | Definition of normal speed, 100% and maximum | The speed needed to attain the | The definitions help to flush out |
| 1.5.26 | continuous speed, plus others of interest. | highest head at any operating | any anomalies in deciding the |
| | | condition. If the speed at the | shop performance test |
| | | normal point is capable of | parameters. "MCS" or maximum |
| | | meeting all the requirements at | continuous speed is 105% of the |
| | | the other operating conditions, | highest speed required to meet |
| | | normal speed will be taken as | any of the specified operating |
| | | 100% speed. | conditions. This sets the values |
| | | | for the mechanical performance |
| | | | test and the over-speed test. It is |

| | | | important from the point of view |
|--------|------------------------|----------------------------------|------------------------------------|
| | | | inspection and NDT examination. |
| 1.5.25 | Normal operating point | The point at which usual | |
| | | operation is expected and | |
| | | optimum efficiency is desired. | |
| | Rated Point | Obtained by the intersection of | Important to identify before |
| | | 100% speed lie and highest | ordering or before approval of |
| | | capacity during operation | inspection documents. Definition |
| | | | of guarantee point is required. |
| 1.5.30 | Stability | Stability is the difference in | Important criterion for the design |
| | | capacity between rated capacity | of the anti-surge system and for |
| | | and surge point at rated speed. | defining operating flexibility. |
| 1.5.51 | Turndown | Turndown is the percentage of | The amount of recycle volume |
| | | change in capacity between the | and thus loss of power at low- |
| | | rated capacity and surge point | flow operating conditions will be |
| | | capacity at rated head with unit | an important factor when it |
| | | operating at rated suction | comes to a continuous mode. |
| | | temperature and gas | |
| | | composition. | |
| 1.5.39 | Settling-out pressure | Pressure of compressor system | It is important to state the same |
| | | when the machine is shut down. | when handling gas that has |
| | | | substantial change in the vapor |

| | | | pressure for a small change in |
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| | | | the temperature. |
| 1.6.1 | Referenced Publications | Identifies major standards | Look for completeness and keep |
| | | covering driver, pressure vessels, | deviations from applicable |
| | | instrumentation, electrical | standard to bare minimum. |
| | | equipment, auxiliary equipment, | Apply piping standards without |
| | | auxiliary systems, piping, and | compromising good layout; |
| | | material specifications | access; pipe supports; upstream |
| | | | interstage, and downstream |
| | | | piping; drains; platform; and |
| | | | grating. Be especially vigilant in |
| | | | instances in which the |
| | | | compressor is delivered as a |
| | | | standard package. On many |
| | | | occasions, comments start |
| | | | pouring in after contract award. |
| | | | Note that similar considerations |
| | | | should apply to instrument |
| | | | tubing and piping. Note cabling, |
| | | | junction boxes, and fire |
| | | | protection systems for which the |
| | | | user company may have |

| | | | developed an overall strategy |
|-----------------|------------------------------------|-------------------------------------|------------------------------------|
| | | | based on decades of field |
| | | | experience. These strategies may |
| | | | be more comprehensive than |
| | | | those of the compressor |
| | | | manufacturer. |
| 2.1.1.3 | Acceptance Criteria | No negative tolerance on the | The process industry places |
| | | capacity and head at normal | emphasis on throughput with |
| | | point of operation with +4% | lower priority on power |
| | | tolerance on power | consumption. However, the user |
| | | consumption. | should identify the guarantee |
| | | | point at the time of purchase if |
| | | | performance tests are |
| | | | contemplated. This will avoid |
| | | | disputes while acceptance tests |
| | | | are in progress. |
| 1.5.17 and | Maximum allowable working pressure | At least equal to relief valve | The manufacturer should be |
| 2.3.1.1.1; also | | setting, or at least 1.25 times the | requested to state this, with no |
| 2.3.1.2 | | maximum discharge pressure | relationship to the actual service |
| | | (gauge) experienced during | condition. This will be useful if |
| | | operation. Maximum pressure | future conditions should require |
| | | occurs when the machine | more head. Heavier casing also |

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| | | operates at maximum continuous | guarantees less susceptibility to |
| | | speed close to surge with | changes due to piping loads and |
| | | anticipated combination of | its effect on machine alignment. |
| | | highest molecular weight, | Observe adequacy for settling- |
| | | highest suction pressure, and | out pressure. |
| | | lowest inlet temperature. | |
| 2.1.1 | Head and capacity characteristic curve | Rising characteristics up to the | Desirable from the point of view |
| | | surge point; may be defined in | of anti-surge and general flow |
| | | percentages | control since there is change in |
| | | | head for a change in the capacity |
| | | | over the entire operating range. |
| 2.3.1.5 | Axial split casing joint | Metal-to-metal joint | This is an important point to be |
| | | | remembered by maintenance |
| | | | organizations. A predefined |
| | | | sequence of tightening bolts, |
| | | | preferably with a hydraulic |
| | | | torque device, will avoid costly |
| | | | assembly errors in the future. |
| | Diaphragm cooling | Independent cooling passages | Precludes entry of cooling |
| | | | medium into compressor casing. |
| 2.5.3.1 | Raw material for the shaft | For 8" and above, the starting | Heat-treated forgings are the |
| | | point shall be a forging. Although | preferred raw material from the |
| | | | |

| | | even below this limit it is | point of view of strength and |
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| | | preferred to use a forging, | stress-concentration factors. |
| | | experienced manufacturers may | |
| | | be permitted to start with | |
| | | quality-controlled bar stock. | |
| 2.5.10.6 | Balancing | Use of welding as a means to | Welding can introduce flaws, in |
| | | balance an impeller is not | addition to difficulties in |
| | | permitted. | controlling the mass. |
| | | | Maintenance engineers must |
| | | | strictly observe this rule. |
| 2.5.4.1 | Balance Chamber Pressure | Provision is required | Found missing in many |
| | | | installations. Trending this |
| | | | pressure gives a good indication |
| | | | of casing internal leakage. |
| 2.7.1.3 | Inlet oil temperature | If it exceeds 49°C, special | In desert atmospheres and with |
| | | considerations are required. | fin fan coolers, oil header |
| | | | temperatures range in the |
| | | | vicinity of 55°C and bearing metal |
| | | | temperatures above 115°C |
| | | | (summer conditions). Consider a |
| | | | closed or thermosiphon water |
| | | | cooling system. |

| 2.6.2.10 | Separation margin | The damped unbalanced | These paragraphs represent |
|----------|-------------------|------------------------------------|-----------------------------------|
| | | response analysis shall indicate | guidelines to obtain an |
| | | that the machine will meet the | acceptable rotor design. Also, it |
| | | following SM: | calls for the verification of the |
| | | a. If the AF at a particular | calculated results on the test |
| | | critical speed is less than 2.5, | stand. |
| | | the response is considered | |
| | | critically damped and so no | |
| | | SM is required. | |
| | | b. If the AF at a particular speed | |
| | | is 2.5 or greater and that | |
| | | critical speed is below the | |
| | | minimum speed, the SM (as a | |
| | | percentage of the minimum | |
| | | speed) shall not be less than | |
| | | the value from Equation | |
| | | below or the value of 16 | |
| | | whichever is less. SM= 17{1- | |
| | | [1/(AF-1.5)]}. | |
| | | c. If the AF at a particular | |
| | | critical speed is equal to 2.5 | |
| | | or greater and that critical | |
| | | speed is above the maximum | |

| | | continuous speed, the SM (as | |
|---------|---|---------------------------------|----------------------------------|
| | | a percentage of the | |
| | | maximum continuous speed) | |
| | | shall not be less than the | |
| | | below or the value of 26 | |
| | | whichever is less. | |
| | | SM=10+17 {1-[1/(AF-1.5)]} | |
| 2.6.3 | Shop verification of unbalanced response analysis | Outlines the importance of | The deviation in the results |
| | | verification of the theorical | beyond permissible limits helps |
| | | results with the ones actually | to form guidelines. It gives the |
| | | obtained on the test stand. | designer more insight in |
| | | | correcting the assumptions and |
| | | | thus can improve overall |
| | | | prediction capability. |
| 2.6.8.1 | Balancing | Does not necessarily specify | During the mechanical running |
| through | | desirable high-speed balancing. | test of the machine, assembles |
| 2.6.8.8 | | | with the balanced rotor, |
| | | | operating at its maximum |
| | | | continuous speed or at any other |
| | | | speed within the specified |
| | | | operating speed range, the peak- |
| | | | to-peak amplitude of the |

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| | | | unfiltered vibration in any plane, |
| | | | measured on the shaft adjacent |
| | | | and relative to each radial |
| | | | bearing, shall not exceed the |
| | | | following value or 25 micrometer |
| | | | (1mil), whichever is less: In SI |
| | | | units: A=25.4 (12000/N) ^{0.5} where |
| | | | A= amplitude of unfiltered |
| | | | vibration, in micron (mil) true |
| | | | peak-to-peak, N= maximum |
| | | | continuous speed, in rpm. At any |
| | | | speed greater than the maximum |
| | | | continuous speed, and up to and |
| | | | including the trip speed of the |
| | | | driver, the vibration level shall |
| | | | not increase more than 12.7 |
| | | | micron (0.5mil) above the |
| | | | maximum value recorded at the |
| | | | maximum continuous speed. |
| 2.2 | Materials | Steel casing to be used as per | Review appropriate guidelines |
| 2.2 | Iviateriais | - | |
| | | guidelines clauses. Disallow | for material selection. |
| | | materials susceptible to brittle | |

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| | | fracture at ambient temperature. | |
| | | In case of H ₂ S (sour) | |
| | | environment, ferrous material | |
| | | selection must be limited to | |
| | | those having maximum yield | |
| | | strength of 90,000 psi and RC22 | |
| | | maximum hardness. Austenitic | |
| | | stainless steel should not be used | |
| | | in services likely to experience | |
| | | stress-corrosion cracking. For | |
| | | hydrogen service with partial | |
| | | pressure in excess of 100 psi or | |
| | | over 90 molal percent H ₂ , | |
| | | impeller material yield strength | |
| | | shall not exceed 120,000 psi and | |
| | | hardness RC34. | |
| 3.1.4, 3.1.5, | Driver Sizing | 110% of the maximum power | For steam turbines, consider |
| 3.1.7 | | required at any operating | future upgrade requirements. |
| | | condition, inclusive of coupling | Are two-sided shaft extensions |
| | | and gear losses for motors and | possible? Is space available for a |
| | | steam turbines. Determination | helper turbine? |
| | | to be made by mutual agreement | |
| | | to be made by mutual agreement | |

| | | for gas turbine drivers. | |
|---------|----------------------------------|--|--|
| 3.2 | Gear couplings | | Lubricated gear couplings are not normally provided on new installations. Contoured diaphragm or flexible disc couplings are preferred but must have prior experience. On older machines with gear couplings, consider, replacement with con- toured diaphragm couplings. |
| 3.5.1.4 | Provision of bypass for flushing | Applicable to bearings and seals | This aspect should be carefully reviewed. Flushing with minimum effort may be difficult unless suitable provisions are designed-in. |
| 4.3.3 | Impeller overspeed | At 115% of MCS for a minimum duration of one minute. | Check the impeller for deformation and dimensional variations. Are runway situations possible in variable speed applications? |

| 4.3.6 | Mechanical running test | lm | portant point to note: | A mechanical running test is |
|-------|-------------------------|----|-------------------------------|--------------------------------------|
| | | 1. | Minimum degree of filtration | mandatory both for the main |
| | | | 10 microns or better. | rotor and spare rotor. It assists in |
| | | 2. | Test with contract items to | determining mechanical losses. |
| | | | include coupling, vibration | Try to use lube-oil grade |
| | | | transducers, seals, bearings | equivalent to type used at |
| | | 3. | Observation and recording of | installation site and maintain |
| | | | several parameters at 10% | highest permissible lube-oil inlet |
| | | | speed increments up to MCS | temperature during shop testing. |
| | | | to include oil supply rate to | |
| | | | every line, pressure, | |
| | | | temperature, sour seal oil | |
| | | | rate. | |
| | | 4. | Run the machine at trip | |
| | | | speed for 15 minutes, | |
| | | | followed by a four-hour run | |
| | | | at MCS. | |
| | | 5. | Collection of vibration | |
| | | | spectra at each operating | |
| | | | point, also during start-up | |
| | | | and coast-down. | |
| | | 6. | Identification of lateral | |
| | | | critical speeds, separation | |

| | | margins, and any testing to | |
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| | | be done in the context of | |
| | | unbalance response analysis. | |
| 4.3.7 | Leakage test | After completion of mechanical | Will ensure integrity of the casing |
| | | running test, casing along with | joint. Inert gas (N₂) is |
| | | seal will be pressurized to | recommended. Helium gas is |
| | | maximum sealing (or seal design | recommended for low molecular |
| | | pressure). Also, casing shall be | weight gases. |
| | | pressurized to rated discharge | |
| | | pressure (with or without end | |
| | | seals). | |
| 4.3.8 | Optional Tests | Various test ranging from | All tests should be carried out at |
| | | performance test (4.3.8.1) to | the manufacturer's facility in |
| | | dismantling and reassembly | order to minimize site problems. |
| | | (4.3.8.8). Inspection to be | This is an opportunity for |
| | | defined under this optional | owner's representative to |
| | | category. | become familiar with equipment. |
| | | Full-pressure/full-load/full-speed | Beneficial a high-pressure |
| | | test (4.3.8.6) | applications in which seals can |
| | | | act as additional bearings and |
| | | | thus can affect the critical speed. |
| 4.4.3.10 | Preparation for shipment | Spare rotor | Preserved with rust-preventive |
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| | coating and stored vertically to |
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| | avoid bowing. Preferably located |
| | in humidity-controlled location. |
| | |

Thanks To: Late Heinz P. Bloch, Book: Compressors and Modern Process Applications